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PRELIMINARY RESULTS OF RECENT GEOLOGIC INVESTIGATIONS IN THE HOMER-KACHEMAK BAY AREA, COOK INLET BASIN, ALASKA: PROGRESS DURING THE 2006-2007 FIELD SEASON

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- Front cover. Outcrop of early Pliocene age conglomerate of the Sterling Formation along the west side of the Fox River, north of Kachemak Bay, in the Kenai National Wildlife Refuge. Approximately 45 m of conglomerate is shown; conglomerate is overlain by interbedded sandstone and siltstone in the upper third of the exposure. Conglomerates are interpreted as part of an alluvial fan, or fan complex, that prograded basinward (west) from sources in the western Chugach Mountains (McHugh Complex). View toward the west. Photograph by Marwan Wartes (DGGS).
- Left inset. Clast-supported pebble and cobble conglomerate with lens of coarse-grained, poorly sorted sandstone. Photo was taken at an exposure of conglomerate approximately 0.5 km downstream from the conglomerate shown in the cover photo. Conglomerates were deposited during flood events in an alluvial fan, or associated proximal braided fluvial setting, possibly as hyperconcentrated flood flow deposits. Photograph by Marwan Wartes (DGGS).
- Right inset. Close-up view showing the clast fabric in the conglomerate bed above the sand lens visible at geologist's head level in left inset photo. Note the poor sorting, sandy matrix, and distinct granitoid clasts. This fabric is typical of the conglomerates in these exposures. The granitoid clasts were probably derived from intrusive bodies in the accretionary wedge to the east (western Chugach Mountains). A 52.1 Ma (±0.2 Ma)⁴⁰Ar/³⁹Ar age on biotite from one of these granitoid clasts suggests derivation from near-trench intrusive bodies in the accretionary wedge. Photograph by Marwan Wartes (DGGS).



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FOREWORD

Dave LePain

The Alaska Division of Geological & Geophysical Surveys, in collaboration with the Alaska Division of Oil & Gas, is engaged in a multi-year analysis of Cook Inlet basin that began in May 2006. This program is being implemented in two phases. The focus of Phase I is the stratigraphic trap potential of Tertiary strata in upper Cook Inlet; the focus of Phase II is the reservoir and source rock potential of middle Jurassic through Maastrichtian rocks of the Peninsular terrane. The chapters in the volume represent preliminary results from fieldwork conducted in September 2006 and May 2007 on the Kenai Peninsula.

- Chapter A by LePain and others presents a facies analysis of the Tyonek, Beluga, and Sterling Formations in exposures on the Kenai Lowland and between Seldovia and Coal Cove (Port Graham). This report includes detailed measured stratigraphic sections of these formations. Lateral facies changes are documented in incised valley-fill deposits of the Tyonek Formation between Barabara Point and Coal Cove. In this area the Tyonek Formation is limited to small paleovalleys that were eroded into older metamorphic rocks of an emergent accretionary wedge (McHugh Complex., Chugach terrane). Lateral facies changes in bluff exposures of the Beluga and Sterling Formations are also documented and used to highlight contrasting sand body geometries in these units. Includes Appendix A, pages 33–97.
- Chapter B by Finzel and others presents a more detailed facies analysis of the Tyonek Formation occupying a
 paleovalley cut into the Chugach terrane between Seldovia and Barabara points. This work documents a significant
 change in sediment composition up-section in the valley fill; near the base of the valley fill, sediment composition
 reflects derivation from local sources in the underlying Chugach terrane, whereas higher in the valley fill, sediment composition and textures suggest derivation from more regional sources and transport in a large drainage
 network. The latter part of the valley fill appears to represent the transition from valley-confined sedimentation
 to axial fluvial depositional systems located basinward of the incised valley network.
- Chapter C by Blodgett and others presents a brief description of a one-day field trip to exposures of Mesozoic strata in Port Graham and at Point Naskowhak. Preliminary fossil identifications are presented, along with their age significance. Well-preserved and lightly abraded bivalves in sandstones that include features suggestive of rapid deposition in relatively deep water indicate short transport paths between the shallow water source area for the fauna and the depositional site.
- Chapter D by Loveland presents mercury injection capillary pressure data generated by George Bolger at PetroTech Associates, Houston, TX, from outcrop samples collected from the Beluga and Sterling Formations. Nearly all samples are tied to measured stratigraphic sections, which provide facies context for the data. Most of our measured sections are presented in Appendix A of Chapter A (LePain and others, this volume). The sample number includes the measured section number and the stratigraphic position of the sample in the measured section. For example, sample 07JRM005-16.5 was collected 16.5 m above the base of measured section 07JRM005 (fig. A11, Appendix A, LePain and others, this volume).

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FACIES ASSOCIATIONS, SAND BODY GEOMETRY, AND DEPOSITIONAL SYSTEMS IN LATE OLIGOCENE–PLIOCENE STRATA, SOUTHERN KENAI PENINSULA, COOK INLET, ALASKA: REPORT ON PROGRESS DURING THE 2006–07 FIELD SEASONS

by

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INTRODUCTION

This preliminary report is a summary of progress made during the 2006–07 field seasons reconstructing depositional systems in Tertiary strata exposed in the Homer–Kachemak Bay area (fig. 1). This work is part of a Cook Inlet basin-wide effort to reconstruct depositional systems for use as a predictive tool in oil and gas exploration. The resulting framework will provide the context for evaluating sand body geometries, their internal heterogeneities, and compositional parameters controlling reservoir quality. The study area addressed in this report extends from Clam Gulch in the north to Coal Cove in the south. Tertiary strata in this area are only mildly deformed and provide a relatively clear view of depositional systems and sand body geometries along the eastern basin edge and their change from basin edge to more basin axial positions.

Quaternary deposits blanket Tertiary strata throughout most of the Kenai lowland and exposures are limited to coastal bluffs and isolated river cuts (Magoon and others, 1976; Bradley and others, 1999; fig. 2). Oligocene to Pliocene age strata in the study area consist of the Tyonek, Beluga, and Sterling Formations (fig. 3). Rocks assigned to the Tyonek Formation are exposed in aerially restricted coastal exposures between Barabara Point (northeast of Seldovia Bay) and Coal Cove (north side of entrance to Port Graham, fig. 2). The Beluga Formation is present in bluff exposures northwest of Homer and along the northwest shore of Kachemak Bay. The Sterling Formation crops out along the northwest shore of Kachemak Bay, north of Kachemak Bay along the Fox River, along Deep Creek, and along the east shore of Cook Inlet.

Measured stratigraphic sections and stitched digital photos acquired by the Alaska Division of Geological & Geophysical Surveys and the Alaska Division of Oil & Gas during the 2006–07 field seasons form the dataset upon which the preliminary interpretations presented in this report are based. Selected measured stratigraphic sections are presented in page format in an appendix at the end of this chapter; locations of measured sections are summarized in Table A1. Outcrop spectral gamma data were acquired for most of these measured sections, but are not included here pending further analysis of their significance.

REGIONAL GEOLOGY

Cook Inlet basin is part of a northeast-trending collisional forearc basin that extends approximately from Shelikof Strait in the southwest to the Wrangell Mountains in the northeast (fig. 1). The basin is bounded on the west and north by granitic batholiths and volcanoes of the Aleutian volcanic arc and Alaska Range, respectively, and on the east and south by the Chugach and Kenai mountains, which represent the emergent portion of an enormous accretionary prism (Haeussler and others, 2000; Nokleberg and others, 1994). High-angle faults, including the Bruin Bay, Castle Mountain, and Capps Glacier faults modified the west and north sides of the forearc basin (fig. 1) and juxtapose different age Mesozoic and Cenozoic sedimentary formations against each other and against arc-intrusive bodies (for example, Barnes and Cobb, 1959; Magoon and others, 1976). The Border Ranges fault bounds the east side of the forearc basin (fig. 1) and juxtaposes Mesozoic sedimentary rocks of the Peninsular terrane against highly deformed and metamorphosed Mesozoic rocks of the accretionary prism, assigned to the Chugach terrane (for example, Magoon and others, 1976; Bradley and others, 1999).

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Figure 1. Landsat image showing Cook Inlet from just south of Augustine Island (lower left corner of image) to the southwestern corner of the Talkeetna Mountains (northeastern corner of image). Major faults that either bound the Tertiary basin and/or cut the Tertiary stratigraphy are shown in red with fault names in yellow. The white rectangle outlines the study area addressed in this report.



Figure 2. Map showing the generalized distribution of Tertiary formations in the study area and outcrop locations discussed in this report. The geology was taken from Magoon and others (1976).

Mesozoic strata of the Peninsular terrane represent the foundation upon which the Cenozoic forearc basin developed. The Peninsular terrane has been interpreted as part of a microcontinent that accreted to inboard terranes during Cretaceous time (Nokleberg and others, 1994; Plafker and others, 1989, 1994). The terrane consists of late Paleozoic through Mesozoic rocks having a regional composite thickness of nearly 12,200 m (Kirschner and Lyon, 1973). Mesozoic strata extend continuously at depth under Tertiary nonmarine deposits and are exposed along the upturned western and eastern margins of the forearc basin (Fisher and Magoon, 1978; Magoon and Egbert, 1986). Mildly deformed late Cenozoic nonmarine strata unconformably overlie Mesozoic strata and depositionally onlap Mesozoic strata along the eastern margin of the basin (Swenson, 2002). Tertiary nonmarine strata, which are up to 7,620 m thick in the axial region of the basin (Boss and others, 1976), consist of a complex assemblage of alluvial fan, axial fluvial, and alluvial floodbasin depositional systems (fig. 3; Swenson, 2002).



Figure 3. Simplified stratigraphic column showing Tertiary nonmarine formations in Cook Inlet basin. The vertical transparent red rectangle shows the stratigraphic focus of this report. Modified from Swenson (2002).

PREVIOUS WORK ON TERTIARY STRATA

Stratigraphy

Stratigraphic nomenclature applied to Tertiary strata in the Cook Inlet region has evolved since Dall and Harris (1892) first proposed the name Kenai Group for coal-bearing sediments exposed on the southern Kenai Peninsula. Dall (1898) subsequently extended the group to include similar strata from as far north as Norton Sound to as far south as British Columbia. Subsequent usage was more restrictive, including only the coal-bearing strata on the Kenai Peninsula (Calderwood and Fackler, 1972). Barnes and Cobb (1959) mapped and described coal-bearing strata in the Homer district and referred to these rocks as the Kenai Formation. Exploratory drilling for hydrocarbons in the 1950s and 1960s demonstrated that the thickness of Tertiary strata in the basin significantly exceeded the thickness of coal-bearing strata exposed on the Kenai Peninsula (Calderwood and Fackler, 1972). For this reason Calderwood and Fackler (1972) formally elevated the unit to group rank and defined five formations, each with subsurface type sections, as comprising the Kenai Group. From oldest to youngest these include the West Foreland Formation, Hemlock Conglomerate, Tyonek Formation, Beluga Formation, and Sterling Formation (fig. 3).

Subsequent work led Boss and others (1976) to restrict the Kenai Group to three formations (Tyonek, Beluga, and Sterling) on the basis of an interpreted unconformable relation between the West Foreland and overlying Tyonek Formation. These authors considered the Hemlock Conglomerate to be a member of the Tyonek Formation.

Calderwood and Fackler (1972) correlated two subsurface formations to surface exposures on the Kenai Peninsula. They correlated the subsurface Beluga Formation with the type locality for Wolfe's (1966) Homerian floral stage, and correlated the subsurface Sterling Formation with the type locality for Wolfe's Clamgulchian floral stage. Kirschner and Lyon (1973, fig. 11, p. 403) show isopach maps with generalized locations where these formations crop out at the surface. A geologic map compiled by Magoon and others (1976) showed the distribution of the Beluga and Sterling in outcrop, as well as aerially restricted exposures of Tertiary rocks along the coastline southwest of Homer, between Barabara Point and Coal Cove. These exposures include reference localities for Wolfe's (1966) Seldovian floral stage and were mapped as Tyonek by Magoon and others (1976).

Many geologists have investigated the stratigraphy and environmental significance of parts of the Tertiary succession in outcrop around the basin. Barnes and Cobb (1959) mapped Tertiary rocks on the Kenai Peninsula as part of an effort to evaluate the coal resources of the region. Wolfe (1966) and Wolfe and others (1966) defined three provincial floral stages based on plant megafossils recovered from Tertiary exposures on the southern Kenai Peninsula. The Seldovian stage was based on plant megafossils collected in the vicinity of Capps Glacier on the northwest side of the basin and Seldovia Point on the southeast side of the basin. The Seldovia Point flora was interpreted by Wolfe and Tanai (1980) as an early to middle Miocene warm temperate assemblage. Wolfe and others (1966) noted that the Seldovian flora could extend back in time to late Oligocene. The Homerian stage was based on plant megafossils collected from exposures along the west shore of Kachemak Bay and immediately west of Homer and was interpreted as a cool-temperate assemblage of late Miocene age. The Clamgulchian stage was based on fossils collected from bluff exposures at Clam Gulch, on the east shore of Cook Inlet, that Wolfe and others (1966) interpreted as a cool temperate assemblage of probable Pliocene age. These workers provide no information on the depositional systems responsible for depositing the Tertiary successions they studied.

Reinink-Smith (1990, 1995) used K-Ar techniques to date tephra layers in Tertiary strata along the east shore of Cook Inlet (Sterling Formation) and along the west shore of Kachemak Bay (Beluga and Sterling Formations). Reinink-Smith concluded that the lower Beluga and lower Sterling Formations were deposited during periods of increased volcanic activity in the basin more than 10.5 m.y. and approximately 7.5 m.y. ago, respectively. Reinink-Smith's focus was to use tephra layers as correlation tools and her work did not address the depositional settings of the Beluga and Sterling Formations.

Dallegge and Layer (2004) used the ⁴⁰Ar³⁹Ar method to date 37 tephra beds in the Beluga and Sterling Formations in outcrop on the Kenai Peninsula and a single altered tephra sample from the Tyonek Formation in core from well 14CC in the Pioneer Unit in the Matanuska Valley. Their work demonstrates the existence of numerous high-angle faults in outcrop, some with significant displacements, which would otherwise be difficult to recognize due to poor exposures. The single date they obtained from the Tyonek Formation yielded a weighted mean age of 48.65 \pm 2.31 Ma (early Eocene).

Depositional Systems and Provenance

Flores and others (2004) examined the Tyonek Formation between Barabara Point and Seldovia Point. They recognized that Tyonek strata at the southwestern end of this exposure represented the fill of an incised paleovalley. Bradley and others (1999) also recognized the paleovalley-filling nature of these deposits. Stricker and Flores (1996) suggested a tidal influence on strata above the paleovalley fill succession (east of Seldovia Point), but did not explain the basis for their interpretation. Flores and others (1994, 1997) examined the Tyonek Formation in exposures on the northwest side of the basin, along Chuit Creek and the Chuitna River. In that area they interpreted Tyonek sand bodies as the product of braided streams that were flanked by floodplains and mires. They suggested a tidal influence on floodplain mudstones in this area and subsequently recognized several tide-influenced facies in cores from the Diamond–Chuitna project area (a few miles east of Chuit Creek), including tidal sand flat, tidal marsh, and tidal channel deposits (Flores and others, 1997). Hite (1976) provided a regional interpretation for the Tyonek as the product of alluvial fans, fan deltas, and estuarine processes, but did not discuss the Tyonek in the Seldovia–Coal Cove area.

Hayes and others (1976) examined exposures of the Beluga and Sterling Formations on the Kenai Peninsula. They interpreted the Beluga as the product of alluvial fans and braided fluvial streams that flowed westward from the Kenai–Chugach mountains. They interpreted the Sterling as the product of moderately large meandering streams that flowed south to southeastward in the area of the Kenai–Peninsula. These authors noted that the Beluga was composed mainly of metasedimentary rock fragments from the Kenai–Chugach mountains and that Sterling

sandstones were composed of quartz, plagioclase, and volcanic rock fragments derived from the Aleutian-Alaska ranges to the north and west.

Boss and others (1976), in a paper describing the Middle Ground Shoal oil field, noted the time-transgressive nature of the Beluga and Sterling Formations, interpreted the Beluga as a "waste basket" stratigraphic unit, and interpreted the Sterling as the product of braided streams possibly similar to present-day streams in the area. These authors described the Tyonek as consisting of massive fluvial sandstones, floodplain shales, and thick coals, but did not provide details on fluvial style (for example, braided or meandering). Interestingly, they claimed to recognize tillites in the Beluga and Sterling Formations that they infer were deposited by glaciers originating in the Kenai Mountains (their fig. 5).

Rawlinson (1984) examined exposures of the Beluga and Sterling Formations along the west shore of Kachemak Bay. He interpreted the Beluga (referred to as Homerian stage beds in his paper) as the product of braided and meandering streams flanked by natural levee, floodplain, and flood-basin deposits. Beluga streams flowed westward and northwestward from the Chugach–Kenai mountains. He interpreted the Sterling (Clamgulchian in his paper) as the product of meandering streams that were flanked by overbank deposits similar to those recognized in the Beluga. Sterling rivers flowed down the regional paleoslope toward the west–northwest. Rawlinson (1984) confirmed the conclusion of Hayes and others (1976) that the abundance of low-rank metamorphic rock fragments in the Beluga and abundant volcanic grains in the Sterling reflected sources in the Kenai–Chugach mountains and Alaska–Aleutian Range, respectively.

A group of geoscientists working for ARCO in the 1980s and 1990s developed a biostratigraphic and depositional systems framework for Cook Inlet basin. Limited elements of this framework have been published (Swenson, 2002) and include alluvial fans along the western and eastern basin margins that grade basinward to an axial fluvial system. By integrating depositional systems information with detailed palynological analyses they were able to demonstrate the time-transgressive nature of Tertiary lithostratigraphic units (Swenson, 2002, his figures 5 and 6).

Flores and Stricker (1992) interpreted the upper part of the Beluga Formation and lower and middle parts of the Sterling Formation along the west shore of Kachemak Bay as the products of suspended-load anastomosed streams and meandering streams, respectively. They attributed coal deposition to raised mires; they also inferred that the thicker coals in the Beluga were the result of vertical accretion typical of the anastomosed system, whereas thinner coals in the Sterling reflect lateral migration of fluvial channels and resulting interruption of peat deposition. Flores and Stricker (1993) interpreted the Sterling Formation exposures at Clam Gulch as the products of braided streams. They suggested that channel style in the Sterling evolved up-section from bedload-dominated low-sinuosity forms to mixed- and suspended-load forms, but did not mention changes in inferred plan-form geometry.

FACIES ANALYSIS

Twenty-one facies are recognized in exposures of the Kenai Group in outcrop on the southern Kenai Peninsula. These are summarized in table 1 and will not be addressed in more detail in this report. The facies occur in nine facies associations (table 2). A brief description and interpretation of each association is presented below.

Facies Association 1 – Valley Margin Apron DESCRIPTION

Facies association 1 consists largely of matrix-supported conglomerate (Gmm) with subordinate interbedded clast-supported conglomerates of facies Gcm (tables 1 and 2; fig. 4a). Clasts range from granule size to approximately 100 cm, are angular to sub-angular, equant shaped, and are supported by a maroon-colored, argillaceous, silty–sandy matrix (fig. 4b–d). This association is always in contact with underlying Mesozoic bedrock along steeply-dipping surfaces and extends up to 30 m away from this contact (fig. 4a). Clast compositions reflect derivation from nearby Mesozoic lithologies. At Point Naskowhak and Coal Cove clasts were derived from Jurassic volcanigenic rocks of the Talkeetna Formation (Peninsular terrane), whereas at Seldovia Point clasts were derived from sedimentary and volcanic rocks of the McHugh Complex (Chugach terrane).

INTERPRETATION

This association records deposition from cohesive debris flows on small alluvial fans located along steeply sloping margins of paleovalleys incised into underlying bedrock of the Peninsular and Chugach terranes. Angular and sub-angular clast shapes attest to limited transport.

Lithofacies	Code	Description	Interpretation
Gravel–Conglomerate			
Matrix-supported conglomerate	Gmm	Very poorly sorted granule to cobble conglomerate, unstratified, clasts angular to sub-round derived from subjacent bedrock and supported by a clayey, silty, sandy matrix	Plastic to pseudoplastic debris flows and hyperconcentrated flows operating in areas of high relief, typically near basin margin
Clast-supported massive conglomerate	Gcm	Poor to moderately sorted, disorganized granule to boulder conglomerate, clasts sub- angular to rounded, bedding up to 3+ m, laterally continuous and discontinuous	Pseudoplastic debris flows and hyperconcentrated flows operating in areas of high relief near basin margin
Clast-supported crudely bedded conglomerate	Gch	Poor to moderately sorted, disorganized to moderately organized granule to boulder conglomerate, clasts sub-angular to well- rounded, crude horizontal bedding up to 1.5 m thick and laterally discontinuous, locally developed clast imbrication	Longitudinal barforms
Clast-supported planar cross- bedded conglomerate	Gcp	Poor to moderately sorted granule to cobble conglomerate, clasts sub-angular to well-rounded, planar-tangential foresets up to 2.5 m thick and laterally discontinuous over tens of meters	Moderate to large two-dimensional transverse bedforms and delta-like growths on downstream ends of composite bars
Clast-supported trough cross- bedded conglomerate	Gct	Poor to moderately sorted granule to cobble conglomerate, trough cross-bedded in sets up to 2.5 m thick; log and large plant fragments present locally	Moderate to large three-dimensional, sinuous-crested to linguoid bedforms
Conglomeratic lag	GI	Granule and pebble lags up to 20 cm thick overlying scour surfaces at base of sand beds; equant to discoid-shaped extrabasinal clasts and discoid-shaped mudstone ripup clasts, locally consists of only mudstone rip- up clasts	Coarsest grain sizes transported along channel thalwegs; mark bypass surfaces
Sand–Sandstone			
Massive sandstone	Sm	Poorly sorted, very fine to very coarse, beds up to 2 m thick, floating pebbles and cobbles locally	Sediment gravity flows, rapid deposition without tractive transport
Horizontally laminated sandstone	Sh	Very fine to very coarse beds from 0.5 cm to 2 m thick, floating pebbles locally; includes some low-angle lamination	Lower and upper flow-regime plane bed phase; correct choice depends on overall facies context
Ripple cross-laminated sandstone	Sr	Very fine to fine grained, beds to 15 cm thick, locally abundant plant fragments and roots	Lower flow regime, downstream migrating ripples
Planar cross-bedded sandstone	Sp	Very fine to very coarse grained, solitary and grouped sets up to 1.5 m thick, locally pebbly	Lower flow regime two-dimensional bedforms with relatively straight crestline; includes delta-like growths along margins of barforms
Trough cross-bedded sandstone	St	Fine to very coarse grained, in solitary and grouped sets 4 cm to 2 m thick, locally pebbly and pebble line base of some foresets, deformed foresets present locally	Lower flow regime three-dimensional bedforms, sinuous to linguoid crestlines
Convolute bedded sandstone	Scb	Fine- to medium-grained clayey sands, ubiquitous convolute bedding, trough cross- bedding locally visible within convolute beds	Deformation resulting from low permeability and high fluid pressure resulting in fluidization and loss of strength; process may be associated with one or more of the following:

high sedimentation rates, frictional drag at interface between larger bedforms and overlying moving fluid, deformation of oversteepened foreset laminae; origin may be a combination of the above factors

locally

Table 1. Cook Inlet Facies. Facies codes and interpretations significantly modifed from Miall (1996).

Lithofacies	Code	Description	Interpretation
Scour-fill sandstone	Ssf	Very-fine- to fine-grained sand with interlaminated mudstone, laminae as form- concordant scour drape, plant fragments and roots locally abundant	Concave-up erosion surfaces cut during flood events and subsequently draped by fine-grained sediment during low flow conditions
Clay/Silt/Mud Laminated claystone	Fcl	Light gray to dark brown claystone with undisturbed alternating light and dark millimeter-scale lamination	Slow settling from suspension in quiet water setting removed from sources of coarser sediment; deposition in floodplain ponds, lakes, and abandoned fluvial channels; possible seasonal laminae
Massive claystone	Fcm	Light to medium gray claystone, no visible lamination, minor scattered plant fragments, color mottling locally	Rapid deposition during flood events on poorly drained floodplain distal to fluvial channels, poorly developed soils locally; locally developed marshes (paludal)
Laminated mudstone	Fml	Light gray to brown silt and silt-clay mixtures in undisturbed millimeter- to centimeter-scale laminae, darker laminae commonly finer grained; locally ripple cross-laminated	Alternating slow suspension settling and relatively rapid suspension settling during flood event in distal levee and proximal perennially flooded regions of floodplain
Thinly interbedded sandstone and siltstone	Fssl	Interbedded very-fine-grained sandstone and siltstone, bed millimeter to multi-centimeters thick, locally ripple cross-laminated	Upper flow regime plane bed and lower flow regime ripple bed conditions in waning flows depositing sand-silt couplets
Massive mudstone	Fmm	Light gray to brown massive silt, silt-clay, and silt-clay-sand mixtures, commonly micromicaceous, no visible internal structures, sideritic concretions locally abundant and commonly with preserved plant fragments, rooted horizons locally	Rapid deposition during flood events on poorly drained floodplain proximal to fluvial channels, poorly developed soils locally, sparse colonization of depositional surface by land plants
Blocky mudstone	Fmb	Light gray to brown blocky mudstone, common sideritic concretions and rooted horizons; tree stumps in growth position locally	Relatively rapid deposition during flood events in seasonally flooded regions of floodplain, weak to moderate pedogenesis and colonization by land plants and trees
Carbonaceous mudstone	Fcb	Dark brown laminated claystone and mudstone, abundant terrestrial organic material typically preserved as comminuted plant fragments	Alternating suspension settling of clay and fine silt and relatively rapid deposition admixed terrestrial organic material, clay, and silt during flood events affecting perennially flooded region of floodplains
Coal C		Dark brown to black, blocky lignitic to sub- bituminous coal, dull and alternating bright and dull layers common, original plant material commonly recognizable; dispersed volcanigenic mineral crystals and disrupted ash layers common	Swamp; thick low-ash coals probably originated in raised mires, whereas high-ash coals originated in topographically low swamps that frequently received clastic sediment from nearby fluvial sources

Table 1. Cook Inlet Facies. Facies codes and interpretations significantly modifed from Miall (1996)—continued.

Facies codes and interpretations significantly modifed from Miall (1996)

Lithofacies Association	Lithofacies	Geometry	Interpretation
1 Valley margin apron	Gmm, Gcm	Wedge	Colluvial apron and regolith locally at valley margin.
2 Disorganized gravelly braided fluvial	Gcm, Gch, Gct/Gcp, Gmm, Sm, Sh, St., Fsb, and minor coal	Sheet	Paleovalley-fill; hyperconcentrated flow and normal, but flashy stream flow, local sediment sources.
3 Sheetflood-dominated alluvial fan	Gcm, Gch, Sm, Sh, St, and possible Gct or Gcp	Sheet	Basin margin alluvial fans traversed by braided streams flanked by poorly drained floodplains, semi- regional sources.
4 Sandy braided fluvial sheet	Sm/St/Scb, Sh, Sp, Sr, Gl, and minor Fssl	Sheet	Low- to moderate-sinuosity sandy braided streams distal to the basin margin, regional sediment dispersal systems and sources. Abundant Scb at Clam Gulch attributed herein to seismic shaking.
5 Meandering channel fluvial sheet	Sm/St, Sh, Sp, Sr, Ssf, Gl, minor Scb	Broadly lenticular	Moderate- to high-sinuosity meandering streams flanked by prominent poorly drained floodplains.
6 Overbank sheet	Fmm/Fmb, coal; minor Fcm, Fml, Fcl, and Fssl; altered tephra locally	Sheet	Poorly drained floodplains with local ponds and lakes; periodically converted to vast raised mires.
7 Single-thread channel-fill	Sm, St, and Sr	Lenticular	Single-thread, mixed- to suspended- load fluvial channels, limited or no lateral migration.
8 Crevasse channel	Sm, Sh, St, Sr, Ssf	Lenticular	Small single-thread channels. Distinction from association 7 may be artificial.
9 Crevasse splay	Sm, Sh, St, Sr, Fssl, Fmm	Lobate and sheet	Crevasse splay lobes; most likely includes some sheet-like levee deposits.

Table 2. Cook Inlet Facies associations.

*Splay assignment unless able to see channel margins.

**Single-thread and crevasse channels division based on arbitrary size cutoff.



Same as fig. 4C, but at a slightly higher stratigraphic position

Facies Association 2 – Disorganized Gravelly Braided Fluvial DESCRIPTION

Facies association 2 consists dominantly of clast-supported massive conglomerate (Gcm) and horizontally bedded conglomerate (Gch), with subordinate interbedded trough and planar cross-stratified conglomerate (Gct and Gcp), matrix-supported conglomerate (Gmm), massive sandstone (Sm), horizontally bedded sandstone (Sh), and trough cross-stratified sandstone (St), and minor locally developed blocky mudstone (Fmb) and coal (tables 1 and 2). Facies Gcm is most abundant, followed by Gch; both are present as tabular to broadly lenticular lithosomes up to 3 m thick (fig. 5a-b and 6a). Conglomerate beds extend laterally from a few meters to many tens of meters. Thin, laterally discontinuous channel fills of facies Gcm, Gch, and Sm are present locally (fig. 6b). Clast size ranges from 0.3-15 cm, clast shapes are equant to slightly discoidal, and sorting is very poor to poor (fig. 5c-d). Where enough disc-shaped clasts are present, weakly developed imbrication is recognizable locally, but clast fabric in most beds is disorganized. Low-angle sigmoidally cross-bedded gravel (Gcp) and low-angle planar bedded gravel are present locally and grade laterally to facies Gcm and Gch. Interbedded sandy facies are commonly well cemented and project out from outcrop surfaces (figs. 5b and 6a). Sandy facies are present as thin (few centimeters) discontinuous drapes separating conglomerate beds, as thin discontinuous beds up to 1 m thick blanketing conglomerate beds and filling depositional topography on conglomerate beds (fig. 5a, top right) and, less commonly, as laterally continuous sheets separating conglomerate beds (fig. 5a, at geologist's knee level). Amalgamated conglomerate beds are also common (fig. 5a, conglomerate body above thick sand). Poorly preserved plant material is common and well-preserved leaf fossils are present locally as are petrified logs and carbonized plant roots (fig. 5e). Mudstones are locally preserved as discontinuous drapes (fig. 5f).

INTERPRETATION

This association records deposition in low-sinuosity fluvial channels separated by low-relief longitudinal bar forms. Locally developed low-angle cross-bedded conglomerate (Gcp) records lateral or downstream accretion along the margins of larger bars. The disorganized appearance of many conglomerate beds (Gcm) suggests deposition from sediment-laden hyperconcentrated flows (Pierson, 2005) generated during flood events. At Point Naskowhak conglomerates of this association interfinger along the margin of an incised paleovalley with debrites of the valley margin apron association. Minor coal indicates plant colonization or deposition of allochthonous plant matter in low-lying areas (topogenous mires) between active channels or in abandoned channels.

Facies Association 3 – Sheetflood-dominated Alluvial Fan DESCRIPTION

Facies association 3 consists dominantly of facies Gcm, Gch, Sm, Sh, and St. Possible cross-bedded conglomerates belonging to Gct or Gcp were observed in beds at least 2 m thick, but were inaccessible for further analysis. Individual conglomerate beds range from 2 m to at least 6 m thick and erosive bases are common (fig. 7a); thicker conglomerate bodies up to 15+ m probably represent amalgamated successions (fig. 7a). Conglomerate is clast supported, poorly to moderately sorted, with tightly packed poorly sorted sandy matrix. Clast sizes range from granule to 30 cm (fig. 7b). Imbricate clast fabrics are developed only locally (fig. 7c). Conglomerate is typically compact, but weakly cemented to uncemented; well-cemented masses occur widely scattered in most exposures and accumulate as float near the base of steep outcrops of this association. Sandstones are present as lenses up to 2 m thick that extend along local strike for many meters to many tens of meters (fig. 7a) and consist dominantly of facies Sm and Sh, with St locally developed. Sand lenses commonly include scattered floating pebbles and concentrated pebble accumulations 1–2 clasts thick above scour surfaces or along low-angle dipping laminae. In the study area addressed in this report, facies association 3 has only been recognized along the upper reaches of the Fox River (fig. 2), a short distance west of exposures of the Chugach terrane (McHugh Complex).

INTERPRETATION

This association is interpreted as the product of high-gradient, low-sinuosity gravelly braided streams and sheetflood processes. Crudely developed horizontal stratification resembles stratification associated with longitudinal and diagonal gravel bars in modern braided streams (Hein and Walker, 1977) and in gravelly sheetflood deposits (Blair and McPherson, 1994). Disorganized clast fabrics suggest relatively rapid deposition from flows with high sediment concentrations, and possibly from hyperconcentrated flows locally (for example, Pierson, 2005). The geometry of these deposits is unclear and hyperconcentrated flows may have been associated with channelized or un-channelized sheetfloods. Possible Gct or Gcp suggest the presence of large gravel bedforms that represent either in-channel structures or deposition along the slip face (downstream end or lateral margin) of large bar forms.





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Β.

- Figure 6. Outcrop photos of the Tyonek Formation east of Seldovia Point (see fig. 2). Facies exposed near Seldovia Point fill a paleovalley incised into the underlying McHugh Complex.
- A. Interbedded poorly-sorted pebble conglomerate and sandstone similar to the succession at Point Naskowhak (fig. 4a, right side of photo, and fig. 5a). This photograph was taken a few hundred meters east of the photo in figure 5b.
- B. Pebble conglomerate and sandstone channel fills separated by thin tabular mudstones and sandstones east of Seldovia Point. The red lines show shallow channel scour surfaces. This photo was taken east of the location shown in figure 6a.





- Massive (Gcm) and crude horizontally stratified (Gch) poorly-sorted pebble conglomerate. Note the erosive base to the amalgamated conglomerate package overlying the sandstone lens.

 - Poorly organized clast fabric in conglomerate below the sandstone lens in figure 7a. C B
- Locally developed imbricate clast fabric immediately below the sandstone lens in figure 7a.

Facies Gcp/Gct demonstrates that some channels were relatively deep (>>2m). Sandstone lenses represent deposition during the waning stage of flood events as drapes in bar top positions and as minor channel fills (Miall, 1977; Rust, 1972, 1978). Characteristics of facies association 3 and its close proximity (within 0.5 km) to exposures of the Chugach terrane and significant mountainous topography (at least present-day mountainous topography) suggest it represents part of a wet alluvial fan or fan complex.

Facies Association 4 – Sandy, Braided Fluvial Sheet DESCRIPTION

Facies association 4 consists dominantly of facies Sm, St, and Scb, followed in abundance by Sh, Sp, and Sr. Facies Gl is common and occurs in beds up to 30 cm thick. The facies composition of this association appears to differ across the study area. Along the west shore of Kachemak Bay, this association consists largely of subequal amounts of Sm and St, with subordinate Sp, Sh, and minor Scb (fig. 8a–d). In this area the association commonly weathers to form sheet-like sand bodies with a monotonous appearance. Along the east shore of Cook Inlet at Clam Gulch, the association consists predominantly of Scb (fig. 8e) followed in abundance by St, Sh, and Sp, all interbedded to form a complex facies mosaic of sheet-like sand bodies. Between Kachemak Bay and the east shore of Cook Inlet (Clam Gulch), along Deep Creek, the facies makeup of this association appears similar to that noted for Kachemak Bay except that convolute bedding appears more distinctive (greater abundance?; fig. 8d and 8f). In all of these areas facies Scb is made up of deformed versions of St, Sh, and Sp.

Internal low-relief scour surfaces are common and, in outcrops oriented at high angles to paleoflow, they create a complex series of intersecting surfaces, making the internal organization appear complex (fig. 9a). The presence of these surfaces allows sand bodies of this association to be distinguished from sand bodies of association 5 (meandering fluvial channel fill). Extrabasinal clasts from pebble to boulder size (up to 45 cm along the apparent long dimension) are widely scattered throughout this association and appear to "float" in a sandy matrix (fig. 8b). Mudstone rip-up clasts are locally abundant near the base of sand bodies assigned to this association.

Clear fining-upward grain size trends are typically only present in the uppermost few meters of the sandy braided fluvial association where they grade up-section to mudstones and coal of the overbank association. Scour at the base of sand bodies commonly resulted in sand-on-coal contacts. Prominent fining-upward successions are present only locally within some sand bodies where facies Sh, St, Sr, and Fssl overlie concave-upward scour surfaces (fig. 9b).

INTERPRETATION

This association is interpreted as the depositional record of low- to moderate-sinuosity sandy braided streams. The suite of facies recognized is similar to facies described along braided reaches of the modern sandy South Saskatchewan River (Cant and Walker, 1978). Complex internal scour surfaces recognized in some outcrops of this association are similar to surfaces recognized in sandy braided alluvium by Adams and Bhattacharya (2005) and Bristow (1993), and are discussed further in the section addressing stacking patterns and depositional systems. Association with coal and fine-grained overbank facies demonstrates that active channel tracts were flanked by aggrading floodplains. The occurrence of facies Sh, St, Sr, and Fssl above concave-upward scour surfaces are interpreted as the fill of abandoned channels.

Convolute bedding in this association warrants further discussion. Many fluvial systems documented in the literature include examples of soft-sediment deformation. In most systems these features are minor components of the total facies composition. Many examples are attributed to a combination of frictional drag at the sediment–water interface and liquefaction of over-steepened foresets. At Clam Gulch soft-sediment deformation features are ubiquitous and their abundance is not likely attributable to fluvial processes alone. We tentatively suggest that these features are related to liquefaction of clay-rich sands resulting from an external forcing mechanism. Given the Holocene record of repeated major earthquakes (Combellick, 1994), we favor a seismogenic origin for this fabric (for example, Ettensohn and others, 2002), but more work is required to test this hypothesis.

Facies Association 5 – Meandering Channel Fluvial Sheet DESCRIPTION

Facies association 5 consists of a suite of facies similar to those recognized in association 4 (Sm, St, Sh, with subordinate Sr, Ssf, Scb, and Fssl). This association is bounded below by an erosional contact with underlying overbank mudstones and above by a gradational contact with overlying overbank mudstones. The presence of lateral accretion surfaces within this association is the main characteristic that distinguishes it from the otherwise similar sandy braided fluvial association (fig. 9c).





F. Figure 8. Outcrop photos of the Sterling Formation along Deep Creek at location 07MAW03 and near Falls Creek (see

- fig. 2). A. Trough cross-stratified sandstone (St) above thin, discontinuous lag of mudstone rip-up clasts (visible near top of hammer handle) near Falls Creek.
- B. Trough cross-stratified sandstone (St) near the base of a tabular channel sand body near Falls Creek. Note the cobble of granitic/dioritic material and small log to the right of the hammer and immediately above the red-stained sandstone. The contact between the red-stained sandstone and the overlying sandstone corresponds to an erosion surface at the base of an amalgamated sand body.
- C. Horizontally laminated sandstone (Sh) cut by thin, rusty-stained sand-filled dikes at 07MAW03 (fig. 2).
- D. Approximately 12 m of sandstone below an overbank mudstone package. Note the geologist in the lower right for scale. Also note several through-going surfaces that bound prominent sets of planar-tangential foresets (Sp, or St along a trough axis-parallel cut) and horizontally bedded sandstone.
- E. Convolute bedded sandstone (Scb) along Deep Creek (07MAW03).
- F. Convolute bedded sandstone (Scb) at Clam Gulch.



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B.

- Figure 9. Outcrop photos of uppermost Beluga and lower Sterling Formations exposed along the northwest shore of Kachemak Bay and in bluff exposures near Diamond Gulch, northwest of Homer.
 - A. Tabular sand body in the Beluga Formation bounded below by a coal seam approximately 1.5 m thick and above by a gradational contact with overbank mudstone.
 - B. Sand body in the uppermost Beluga–lowermost Sterling displaying prominent accretion surfaces.
 - C. A tabular sandstone body near the base of the Sterling Formation near Falls Creek that terminates in an abandoned channel-fill succession.

U.

INTERPRETATION

This association is interpreted as the record of moderate- to high-sinuosity mixed-load meandering rivers. The close association with mudstones of the overbank association (above, below, and lateral to sand bodies) demonstrates that active channels were flanked by aggrading poorly-drained floodplains. Our interpretation of this facies association is tentative and based on only one location; this location also includes sand bodies assigned to facies association 4. The component facies and lateral accretion surfaces recognized in facies association 5 are not unique to meandering stream deposits, but are also common in sandy braided stream deposits. More work is required to determine if this association is truly different from facies association 4 (for example, includes point bar successions) and whether or not it is the record of high sinuosity streams.

Facies Association 6 – Overbank Sheet DESCRIPTION

Facies association 6 is prominent in most outcrops in the Kachemak Bay area, where it consists predominantly of facies Fmm, Fmb, and coal (fig. 10a–b), with locally important Fcm, Fml, Fcl, Fssl, and altered tephra (fig. 10c). Locally Fml, Fcl, and Fssl comprise facies successions up to a few meters thick in which millimeter-scale laminae are undisturbed by plant roots. The overbank association comprises tabular bodies that envelop several other facies associations, including the fluvial channel fill, crevasse channel fill, and crevasse splay associations.

Lignitic coal seams are a prominent component of this association and range from centimeters to several meters in thickness. Coals commonly include scattered yellow–white crystal clusters up to a few millimeters diameter. Coals appear to be laterally continuous over significant outcrop distances (many hundreds of meters).

INTERPRETATION

This association is interpreted to record deposition during floods beyond the confines of active fluvial channels. Deposition was largely from suspension and over time floodplains aggraded vertically. Facies Fmm and Fmb suggest a poorly-drained floodplain characterized by localized weak pedogenesis. Progradation/lateral migration and vertical accretion of related associations during flood events give the overbank association a more complex appearance. The occurrence of tephras indicates relatively common volcanic eruptions in the arc to the west. Thick, laterally continuous coal seams indicate that vast areas of the floodplain were colonized by dense vegetation, that a delicate balance between peat accumulation and subsidence was maintained for significant periods of time, and that these areas were isolated from clastic input. Scattered yellow–white crystal clusters represent fragments of tephras that were disrupted and dispersed by plant roots (Reinink-Smith, 1990; Dallegge and Layer, 2004).

The lateral continuity of coal seams bounding occurrences of the sandy braided fluvial and meandering fluvial associations suggest that catastrophic subsidence led to establishment of widespread floodplain mires. Alternatively, the lateral continuity of coals below most tabular sand bodies suggests that catastrophic and widespread subsidence shut down peat deposition, resulting in abrupt channel re-establishment (avulsion). We favor the latter interpretation.

Locally important occurrences of Fcl, Fml, and Fssl suggest deposition in floodplain ponds and lakes. Undisturbed millimeter-thick laminae typical of these occurrences suggest deposition from suspension in a low-energy environment in water deep enough to eliminate colonization from terrestrial vegetation. Local intercalations of Fssl and Fcm suggest transport in turbulent suspensions and traction transport of coarser material, possibly associated with small lacustrine deltas located near the margin of floodplain lakes.

Facies Association 7 – Single Thread Channel Fill DESCRIPTION

Facies association 7 consists of a suite of facies similar to those recognized in associations 4 and 5, but Sm, St, and Sr are most abundant (tables 1 and 2). The primary characteristic of this association is its lenticular ribbon to narrow sheet geometry; channel margins are commonly visible in outcrop. Many sand bodies preserve the cross-sectional shape of the original channel (ribbon-like geometry), whereas other bodies record limited lateral channel migration (narrow sheet geometry). Sand bodies are up to 7 m thick and encased in mudstones of the overbank association in laterally continuous exposures of the overbank association typically show overlapping channel fills at different stratigraphic levels (fig. 11).



Figure 10. Outcrop of an overbank succession exposed along the east shore of the Fox River (fig. 2). The age of this succession is unknown, but its location near exposures of the Sterling Formation suggest it is part of this unit.

A. View toward the south showing approximately 12 m of overbank mudstone and thin lignitic coal.



B. Contact between a lignitic coal (even with geologist's head) and an underlying mudstone.

В.



C. Laminated argillaceous mudstone (Fml) shale from the Beluga Formation near Fritz Creek (06PJM04 at 9m).





panel. The Beluga at this location is dominated by overbank mudstone that encases broadly lenticular, single-thread sand-filled channels. The yellow lines show the trace of measured sections through the lower part of the bluff and red lines show channel fill sandstone bodies. Figure 11. Outcrop photomosaics showing stratigraphic details in the Beluga Formation near Fritz Creek (see fig. 2). The right side of the top panel joins to the left side of the lower

INTERPRETATION

Association 7 resembles anastomosed fluvial sand bodies described by Kirschbaum and McCabe (1992), Nadon (1994), and Rygel and Gibling (2006) in that it forms ribbon- and narrow sheet-like sand bodies. It differs from these published examples in that multiple sand bodies have not yet been recognized at the same stratigraphic level in the study area; outcrop examples of this association include overlapping channel sands at different stratigraphic levels. We interpret association 7 as the record of single-thread mixed- to suspended-load channels that experienced limited lateral migration. Our interpretation differs from Flores and Stricker (1992), who interpreted the same exposures as the record of anastomosed fluvial channel fills.

Facies Association 8 – Crevasse Channel DESCRIPTION

Facies association 8 consists of facies Sm, Sh, St, Sr, and minor Ssf. These facies comprise the fill of narrow channels that range from 1 to 3 m thick and 5 m to many tens of meters wide. Channels are encased in the tabular mudstone association. Channel fills of association 8 resemble association 7, but are significantly smaller.

INTERPRETATION

This association is interpreted as a crevasse channel-fill succession. Crevasse channels formed when levees bounding larger meandering(?) trunk channels were breached during flood events (high flow stage). Preliminary data suggest that crevasse channels are more common in overbank deposits that include larger channels of association 7.

Facies Association 9 – Crevasse Splay DESCRIPTION

Facies association 9 occurs encased within mudstones of the overbank association and consists of Sm, Sh, St, Sr, Fssl, and Fm. This association forms sheet-like bodies composed of sandstone–mudstone couplets that range from decimeters to approximately 2 m thick; locally this association consists of amalgamated sand beds, each up to a few decimeters thick. Facies Sm, Sh, and/or St form the base of these couplets; individual sheets can consist of a single couplet or multiple couplets. Plant roots are locally common.

INTERPRETATION

This association is interpreted to record deposition as channel levees and as crevasse splay sheets. Available data do not allow differentiation between splay sheets and levee deposits. We infer that splay sheets probably account for the bulk of this association. Single sand–mud couplets, stacked sand–mud couplets, and amalgamated multi-decimeter-thick sand-on-sand beds likely record distal to proximal variations in crevasse splay deposition.

STACKING PATTERNS AND DEPOSITIONAL SYSTEMS

In this section the facies associations presented above are placed in a depositional systems context. Associations in late Oligocene(?) to early Miocene strata between Barabara Point and Coal Cove are discussed first, followed by middle to upper Miocene strata near Homer, and ending with Pliocene strata along the northwest shore of Kachemak Bay, Deep Creek and Clam Gulch, and the Fox River. Facies and facies associations are identified on the measured sections at the end of this report. Figure 12 is a schematic representation of fluvial style interpreted for formations of the Kenai Group exposed in the study area and will be referred to throughout this section.

Tyonek Formation—Barabara Point to Coal Cove

Late Oligocene to early Miocene strata assigned to the Tyonek Formation fill paleotopographic depressions developed on Mesozoic rocks of the Talkeetna Formation and McHugh Complex between Barabara Point and Coal Cove (fig. 2). This is most clearly demonstrated at Coal Cove and Point Naskowhak, where the accumulations are interpreted as paleovalley fills (fig. 12). At the latter location the valley margin apron association (table 2) rests abruptly with angular discordance above dark green- and maroon-weathering volcanic rocks of the Lower Jurassic Talkeetna Formation (fig. 4a). Debrites of this association interfinger laterally over short distances (5–30 m) with conglomerates of the disorganized gravelly braided fluvial association. Stratigraphically higher debrites clearly backstep (shift away from the paleovalley axis) up the margin of the paleovalley and show an unequivocal onlap relation (fig. 4a). Clast and matrix compositions closely reflect the parent material in the subjacent Talkeetna Formation and were obviously locally sourced. The valley margin apron association represents talus aprons that



Figure. 12. Line drawing illustrating the evolution of fluvial style from late Oligocene through early Pliocene time in the Homer–Kachemak Bay area. Scale is approximate only.

accumulated at the toe of exposed bedrock slopes. Angular clasts and clast-supported fabrics typical of these debrites suggest an origin whereby hill slope colluvium was mobilized during high rainfall events (or seasonal snowmelt) and transported downslope as debris flows. Debrites grade toward valley axes into the deposits of low-sinuosity braided streams responsible for depositing the disorganized gravelly braided fluvial association. The disorganized nature of these conglomerates suggests flashy streams that were prone toward hyperconcentrated flows (for example, Pierson, 2005). Sand lenses and sand drapes were deposited during waning flow stage and during low-flow periods. The paleovalley near Point Naskowhak has an apparent width parallel to the shoreline of 1.7 km. Minimum estimates of the depth of incision are provided by the thickness of Tertiary strata preserved in these exposures: 15 m at Coal Cove (and Point Pogibshi) and at least 30 m at Point Naskowhak.

The succession at Coal Cove is similarly interpreted as a paleovalley-fill succession, but the actual valley walls are poorly exposed. At this location, an interfluve of Talkeetna volcanics separates what are thought to be two narrow paleovalleys, each probably less than 0.5 km in apparent width parallel to the shoreline.

A much thicker Tertiary succession is exposed between Seldovia Point and Barabara Point, east of Seldovia Bay, which is addressed in more detail by Finzel and others (this volume). The Tertiary succession at this location dips gently toward the east and the base is exposed near Seldovia Point where the entire bluff height of approximately 14 m consists of pebble conglomerate and lenticular sandstone of the disorganized gravelly braided fluvial association (fig. 6a). Lithologies present in nearby exposures of the Mesozoic McHugh Complex are recognized as clasts in conglomerate of this association. The contact between Tertiary deposits and underlying Mesozoic rocks is not exposed, but progressive overlap of Mesozoic rocks by Tertiary conglomerate and sandstone is apparent (fig.13a) and supports interpretation of this succession as the fill of an incised paleovalley. Valley margin alluvial apron deposits have not been recognized at this location. The gravelly braided fluvial deposits grade upsection to better organized sandstones and mudstones interpreted as distal sandy braided fluvial (association 4) and floodplain deposits (association 6) that reflect deposition beyond the confines of the paleovalley (Finzel and others, this volume).

In summary, Tertiary rocks mapped as Tyonek Formation include gravelly braided fluvial deposits that filled the axial region of incised paleovalleys that were cut into Mesozoic bedrock of the Peninsular and Chugach terranes. Debrites formed a discontinuous alluvial apron along the valley margin and represent slope colluvium. Between Barabara Point and Seldovia Point locally sourced incised paleovalley fill deposits grade up-section to mixed-load distal braided fluvial deposits that likely extended beyond the confines of incised paleovalleys. Distal braided alluvium near Barabara Point megascopically appears to record sediment derived from more regional sources. Flores and others (2004) reported the occurrence of tidally influenced deposits in the Tyonek between Barabara and Seldovia points but did elaborate. We did not find tide-influenced facies in Tyonek outcrops in this area.

Lower Beluga Formation—Bluff Point to McNeil Creek

Exposures of late Miocene strata in coastal bluffs northwest and northeast of Homer are thought to represent stratigraphic positions relatively low in the Beluga Formation (Adkison and others, 1975). These exposures consist largely of associations 6, 7, 8, and 9 (table 2). The overbank association envelops the fluvial channel fill, crevasse channel, and crevasse splay associations (associations 7, 8, and 9, respectively). Overbank deposits of association 6 dominate these exposures. Figure 11 shows a photomosaic of bluff exposures east of Fritz Creek, on the west shore of Kachemak Bay, that illustrates sand body geometry and the relative abundance of sandy versus muddy associations. Measured section 07JRM01 and 02 intersect relatively thick overbank successions (association 6) with thin crevasse splay sand sheets (association 9). Measured sections 06PM003 and 004 also intersect relatively thick overbank deposits with numerous crevasse splay sheets (association 9) and possible crevasse channel fills (association 8). The fluvial channel-fill association forms broad ribbons to narrow sheet sand bodies that cut into underlying mudstones of the overbank association (figs. 11 and 12). These sand bodies are interpreted as the product of single thread rivers that traversed poorly drained floodplains and did not migrate significant distances laterally. Our interpretations contrast with those of Flores and Stricker (1992), who interpreted the succession near McNeil Creek as the product of suspended-load anastomosed streams.

Bluff exposures northwest of Bluff Point closely resemble exposures of the lower Beluga Formation near Fritz Creek (fig. 14). Measured section 07MAW204 intersects a thick overbank succession (association 6) with numerous crevasse splay and probable crevasse channel sand bodies (associations 8 and 9). The lower Beluga at this location is similar to the succession exposed near Fritz Creek in that overbank deposits represent a prominent part of the depositional system.

In summary, the lower Beluga Formation in the vicinity of Homer and Kachemak Bay is characterized by broad ribbon-like and narrow sheet-like sand bodies bounded by thick, laterally continuous overbank mudstone



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- Figure 13. Outcrop photos of Tertiary strata near Seldovia Point and along the upper Fox River (see fig. 2).
- A. Exposures of the McHugh Complex at beach level overlain by poorly exposed valley-fill strata of the Tyonek Formation.
- *B. Helicopter view toward the west showing early Pliocene alluvial fan deposits of the Sterling Formation very close to the eastern basin margin.*



Figure 14. Outcrop photomosaic illustrating the facies organization of the Beluga Formation west of Diamond Gulch (see fig. 2). The yellow line shows the trace of measured section 07MAW204. The yellow oval encloses two geologists for scale.

successions. These sand bodies are interpreted as the products of single-thread streams that carried a significant percentage of their total load in suspension. Frequent flood events led to accretion of significant thicknesses of overbank mudstones. Locally, numerous small channel fills and thin sheet-like sand bodies suggest that flow in the larger streams frequently broke through their levees to deposit crevasse channel and splay sand bodies. Thick, laterally continuous overbank deposits record deposition in a high accommodation setting.

Upper Beluga Formation to Lower Sterling Formation—Falls Creek

Exposures of latest Miocene to Pliocene strata near Falls Creek on the west shore of Kachemak Bay straddle the Beluga–Sterling formational boundary as placed by Adkison and others (1975). These workers placed the formation contact at the base of a channel sand body exposed just above the beach a short distance northeast of the mouth of Falls Creek (their measured section L5) and noted, "The position of the contact is broadly determined by an upward change in the heavy mineral suites...." Their measured sections are generalized and do not show a gross change in stratigraphy (for example, sand:mudstone) across the position of their contact. This is consistent with our observation that the Beluga–Sterling contact in this region appears gradational based on a gradual change in fluvial style. Related to this gradual change in fluvial style is a gradual up-section decline in the thickness of coal seams.

Exposures of the uppermost Beluga and lowermost Sterling near Falls Creek are characterized by laterally continuous sand bodies up to 12 m thick consisting of the sandy braided fluvial and meandering fluvial sheet associations (association 4 and 5). Overbank mudstones and lignitic coal seams of association 6 form laterally continuous caps (up to 5 m thick) to many sheet sand bodies. Although prominent in these bluff exposures, the overbank association is thinner than exposed in the lower Beluga. Many sand bodies of the sandy braided fluvial association are internally monotonous and consist largely of massive sandstone and trough cross-bedded sandstone (fig. 15). Some sand bodies assigned to association 4 include numerous large, overlapping concave-upward surfaces suggestive of multi-lateral scours typical of sandy braided fluvial deposits (fig. 9a). Sand bodies of the meandering fluvial sheet association include uniformly dipping surfaces indicative of lateral accretion (fig. 9c). The range of internal organization noted here suggests that upper Beluga-lower Sterling rivers included both braided and meandering channel geometries. Although thinner than in the lower Beluga, the presence of laterally continuous overbank deposits (association 6) suggests that rivers were still flanked by prominent floodplains. The reduced thickness of overbank deposits is probably the result of increased erosion from laterally migrating and avulsing river channels. Many thick sand bodies rest in erosional contact on lignite seams, demonstrating that channels scoured down to the level of underlying peat mats, but could not cut through them. Increased erosion and reduced thickness of overbank deposits are attributed to deposition in lower accommodation settings.

Sterling Formation—Deep Creek

Outcrops assigned to the Sterling Formation occur discontinuously along the valley of Deep Creek, west of the Fox River. The stratigraphic position of these exposures in the Sterling is unclear. Flores and Stricker (1993) note that exposures at Clam Gulch represent the upper Sterling Formation, but do not explain the basis for this interpretation. The exposures along Deep Creek are separated from Clam Gulch by at least one major northeast-trending fold and from exposures along the Fox River by at least two major folds (fig. 2; see Magoon and others, 1976). These structures complicate determination of the stratigraphic position of the Deep Creek exposures within the Sterling Formation.

Many exposures consist predominantly of sandstone of association 4 (figs. 15 and 16a) or a combination of association 4 (sandy braided fluvial) and mudstones of association 6 (fig. 16b). The laterally discontinuous nature of these exposures makes classifying sand body geometry and evaluating the lateral continuity of overbank deposits particularly difficult; we infer sheet-like geometries based on comparison with similar sand bodies in the lower Sterling along the west shore of Kachemak Bay.

Intersecting outcrop faces illustrate the internal organization of an amalgamated sand body at location 07MAW03 (fig. 2) and provide insights on fluvial channel style. The outcrop faces shown in figure 16a intersect at a high angle to provide nearly orthogonal views through a multistory and multilateral sand body at least 20 m thick. Three surfaces of different order are visible in both (fig. 16a). One class of surface can be traced across the exposure and correlated between the two faces; these surfaces bound individual stories. The second class of surface is internal to the individual stories and probably bounds bar and channel architectural elements (fig. 16a, left of bend; for example, Miall, 1995). The other class of surface is internal to these elements, cannot be traced significant distances, and probably records slipfaces with smaller-scale dunes that comprise the large bars and channel elements



offsets coal seams by approximately 10 m.





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Figure. 16. Outcrop photos of the Sterling Formation along Deep Creek.

- A. Photomosaic at 07MAW03 showing two intersecting outcrop faces. The left face is oriented at a high angle to paleoflow and the right face is oriented nearly parallel to paleoflow. Note the contrasting organization of facies along these two cuts. Cross-sections perpendicular to paleoflow in sandy braided alluvium typically appear more complex and less organized (left face) than along cuts parallel to paleoflow (right face).
 - Channel-fill succession overlain by overbank mudstones along Deep Creek at 06PD244. С B
 - Trough cross-stratified sandstone (St) at 06PD244.

(fig. 16a, right of bend). The latter two classes of surfaces are characterized by significant complexity: changes in concavity and dip direction over short distances make each story appear internally disorganized. In contrast, the intersecting outcrop face (fig. 16a, right of bend) includes the through-going surfaces that bound stories and surfaces internal to each story. These internal surfaces include relatively few concave-up scours and well-defined dune slip faces that dip consistently toward the right, imparting a more orderly, organized appearance for each story. Although this exposure is of limited extent, the complex surfaces seen on the left half of figure 16a suggest this orientation is close to depositional strike (perpendicular to paleoflow) for this river in this area, and that the right side of image is oriented close to depositional dip (nearly parallel to westerly paleoflow). Strike-oriented exposures through sandy braided alluvium are typically characterized by complex internal surfaces that dip in various directions and lack preferred orientations as expected in meandering streams (Bristow, 1993; Adams and Bhattacharya, 2005).

Sterling Formation—Fox River

Previously unmapped and undated (Cieutat and others, 1992) deposits along the Fox River in the Kenai National Wildlife Refuge consist of conglomerates and lenticular sandstones of association 3 (fig. 13b; wet alluvial fan association). Palynological samples collected during the 2006 field season yielded pollen of early Pliocene age that do not appear to be reworked (Pierre Zippi, unpublished report). These coarse-grained units represent very proximal deposits broadly correlative with the Sterling Formation. Facies recognized in this association (Gcm, Gch, Gcp/Gct, Sm, and Sh) are common in gravelly braided stream environments (tables 1 and 2). The proximity of this association to exposures of deformed and uplifted rocks of the McHugh Complex a few kilometers away suggest these braided streams were associated with a large alluvial fan, or complex of fans, deposited along the Kenai–Chugach Mountain front during Pliocene time. Though not recognized in outcrop in the study area, alluvial fans were probably present along this mountain front in Miocene time and possibly earlier. Clast composition reflects derivation from greywackes, argillites, and bedded cherts in the McHugh Complex to the east. ⁴⁰Ar/³⁹Ar dates from volumetrically minor, but conspicuous, white and black diorite clasts obtained during the present study indicate they were derived from near-trench plutons in the accretionary prism (e.g. Bradley and others, 2003).

DISCUSSION

Outcrop data gathered during the 2006 and 2007 seasons provide insights on the nature of nonmarine depositional systems along the eastern margin of Cook Inlet basin. Late Oligocene to early Miocene strata exposed in coastal bluffs between Seldovia Point and Coal Cove, previously mapped as Tyonek Formation (Magoon and others, 1976; Bradley and others, 1999), record deposition in paleovalleys incised into deformed Mesozoic rocks of the McHugh Complex and Talkeetna Formation. These occurrences of the Tyonek are drastically different than the type Tyonek in the subsurface, or from the Tyonek in outcrop on the northwest side of the basin (see Calderwood and Fackler, 1972, and Flores and others, 1994). Braided streams occupying these valleys transported detritus derived from relatively small, locally sourced catchment areas, were prone to flashy discharge and hyperconcentrated flows, and graded to colluvial aprons comprised of debrites at valley margins. Valley-filling braided alluvium near Seldovia Point grades up-section to sandy braided alluvium attributed to a dispersal system of more regional extent, reflecting deposition more distal to the basin margin (Finzel and others, this volume).

Late Miocene strata exposed in coastal bluff exposures northwest of Homer and along the west shore of Kachemak Bay near Fritz Creek, mapped by Kirschner and Lyon (1973) and Magoon and others (1976) as Beluga Formation, record deposition from suspended-load to mixed-load, high-sinuosity single-thread (anastomosed) rivers. Sand bodies associated with these rivers are narrow sheets to broad ribbons up to 8 m thick encased in overbank mudstones. The high percentage of mudstone and coal in these exposures suggests deposition in high-accommodation settings.

Beluga exposures near Fritz Creek grade up-section over several kilometers of bluff exposures and several hundred meters of section to sheet-like sand bodies up to 15 m thick in the uppermost Beluga and lower Sterling Formations in the vicinity of Falls Creek. Overbank mudstones still form laterally continuous deposits in this area, but are significantly thinner than in the lower Beluga. Sheet-like sand bodies are attributed to low-sinuosity sandy braided rivers; locally visible, well-developed lateral accretion surfaces suggest that meandering streams were also present during this time or, alternatively, that some braid bars also migrated laterally or obliquely. The reduced thickness of overbank deposits is attributed to deposition in low accommodation settings during latest Miocene to Pliocene time in this part of the basin.

Exposures of the Sterling Formation along Deep Creek appear similar to the upper Beluga and lower Sterling Formations along the west shore of Kachemak Bay, but their laterally discontinuous nature precludes more rigorous comparison. One exposure includes two outcrop faces that intersect at a high angle to provide nearly orthogonal cuts through an amalgamated sand body, the details of which suggest deposition in a sandy low-sinuosity fluvial system.

Previously unmapped exposures of conglomerate along the upper reaches of the Fox River contain un-reworked Pliocene palynomorphs. Facies suggest deposition from braided streams that are inferred to have flowed radially down the axis of large wet alluvial fans situated at the basin margin. Within the coarse constraints provided by limited age control, it is reasonable to suggest these fans represent the proximal equivalents to sandy braided alluvium recognized in Sterling Formation exposures along Kachemak Bay and Deep Creek.

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APPENDIX A

No.	Section Name	Location Name	Formation	Latitude	Longitude
1	06PM001	Coal Cove, Port Graham	Tyonek	N59.3942	W151.8925
2	06DL024	Point Pogibshi, Kachemak Bay	Tyonek	N59.41695	W151.88352
3	06PM004	Fritz Creek, Kachemak Bay	Beluga	N59.69571	W151.30385
4	07MAW004	Bluff Point	Beluga	N59.67557	W151.71409
5	07DL002	Bluff Point	Beluga	N59.65911	W151.66521
6	07DL003	Bluff Point	Beluga	N59.65944	W151.66624
7	07DL004	Diamond Gulch	Beluga	N59.65964	W151.66736
8	07JRM001	Fritz Creek, Kachemak Bay	Beluga	N59.69343	W151.31347
9	07JRM002	Fritz Creek, Kachemak Bay	Beluga	N55.69365	W151.3128
10	07JRM003	Fritz Creek, Kachemak Bay	Beluga	N59.6938	W151.31266
11	07JRM005	Fritz Creek, Kachemak Bay	Beluga	N59.69517	W151.30707
12	07JRM006	Fritz Creek, Kachemak Bay	Beluga	N59.69522	W151.30672
13	07JRM008	Fritz Creek, Kachemak Bay	Beluga	N59.6962	W151.30368
14	07JRM009	Fritz Creek, Kachemak Bay	Beluga	N59.70012	W151.29219
15	07JRM010	Falls Creek, Kachemak Bay	Beluga-Sterling	N59.69879	W151.29545
16	07JRM011	Falls Creek, Kachemak Bay	Sterling	N59.77309	W151.12128
17	07JRM012	Falls Creek, Kachemak Bay	Sterling	N59.78246	W151.10204
18	07JRM013	Falls Creek, Kachemak Bay	Sterling	N59.77343	W151.12043
19	07JRM014	Falls Creek, Kachemak Bay	Sterling	N59.77366	W151.12004
20	06PD213	Fox River, Kenai NWR	Sterling?	N59.91270	W150.82426
21	06MAW203	Fox River, Kenai NWR	Sterling	N59.98066	W150.79642
22	06PD244	Deep Creek, southern Kenai Peninsula	Sterling	N59.98250	W151.54721
23	06PD220	Clam Gulch, Cook Inlet	Sterling	N60.24970	W151.39291

Table A1. Locations of measured sections illustrated in Appendix A	•
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Datum is NAD27 Alaska.

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06PM001 Coal Cove, Port Graham N59.3942 W151.8925 Tyonek Formation

Gamma Log	Meter	Measured Section	Facies	Facies Assoc	Key Features	Interpretations
	21-					
	20-					
	19-					
	18-					
	17-					
	16-					
	15-					
			Sm			
			Emb	6		
	90		dm⊣			

06DL024 Point Pogibshi, Kachem N59.43726 W151.80049 Tyonek(?) Formation	ak Bay	
Gamma Log	leters	Mea



06DL024 Point Pogibshi, Kachemak Bay N59.43726 W151.80049 Tyonek(?) Formation

Gamma Log	Meter	Measured Section	Facies	Facie	Key Features	Interpretations
	21-					
	20-					
	19-					
	10					
	10-					
	1/-					
	16-					
	15-		Sm			
			Gmm	2		Hyperconcentrated
						deposits?
90	0		Gmm			











FIGURE A3







Gamma Log	ters	Measured Section	cies	Icies soc.	Key Features	Interpretations
	₩ ₩		Б	As		
d not log						
	34-					
		\prec				
	22	=	Sh			
		-	Fml			
	32-		Coal	0		
	λ	λ	Fmb			
	λ	λ				
	31		Sr/Sh	9		
						Overbank deposits
			Sm			with splay sand sheets
	30 -		FCIII			
			Fmm			
			Coal			
	29 -		Fmb?			
	-					
	_		Sh	9		
9						



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65911 W151.6652 [,] ga Formation	1					Page 3 of
Gamma Log	Depth	Measured Section	acies	acies Assoc.	Key Features	Interpretations
Did not log						
	31		Coal			
			Sm			
	30 -					
		_				
		\equiv				
	29 -	-				
				9?		
			Sh			

sand

_





Gamma Log	eters	Measured Sections	acies	acies ssoc.	Key Features	Interpretations
	W		FE	F.		
	37- 36- 35-		St			
id not log	34 -		Sm Sm			
	33-		Sm Sm		Blocky, irregular fracture pattern	
	32-		Fmb Coal Sm			
	31 -					
	30 -		St?	5?	Low-angle laminae in sets; dip changes between sets	
	29 -					

	S		S	S O		age for
Gamma Log	Mete	Measured Section	Faci	Faci Asso	Key Features	Interpretations
	13 -		St			
			Sm			
	12		Q+			
	12	- LUTALLY				
		000000				
	11 -		St?			
		-//				
	10 -			4?	Rip-up lined scours	Channel sand bodv
		200000000000000000000000000000000000000			,	of unknown plan- view geometry.
						Abundant scours suggest low-sinuosity channels.
	9 -					
			St			
	8.					
		<u>/////////////////////////////////////</u>	Sp			
		1111	- Op			
Did not log	7 -		Sh			
	6					
			St			
	5 -					
					Inclined low-angle lamination	
	4					
	3 -		Fmb			
	2			6		
		0				
	1 -		Coal			
9	5		Fmb			

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07JRM001 Fritz Creek, Kachemak Bay N59.69343 W151.31347 Beluga Formation

Gamma Log	/lete	Measured Section	acie	acie	Key Features	Interpretations
	2		Ľ.	щ∢		
			Coal			
	22 -					
	-	-	Emb			
	_		FIID			
	21		Coal			
	21-		311			
	20 -		Coal			
			Coal			
	19 -			6		
	18 -					
	17 -					Thickness suggests origin as proximal
						crevasse splay, seri of amalgamated
			Sm	9		crevasse splays, or a single crevasse
	16					channel.
			Fml			
	15	/				
	/	\setminus				
		N				



Gamma Log	eters	Measured Section	acies	acies ssoc.	Key Features	Interpretatio
	Σ		Ľ	Ψ<		
	1					
			Coal			
	16 -					
			Coal	9		
	15 -					
				6		





sand

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07JRM006	
Fritz Creek, Kachemak Bay	
Beluga Formation	

3						Faye 2 01
Gamma Log	Meters	Measured Section	Facies	Facies Assoc.	Key Features	Interpretations
	19					
			Coal			
	18	$\langle \rangle$				
	10					
		X				
	47					
	17					
			0.00			
	16		Sm	9		
			Fmm?			
I	15		Coal			
		Le S	St			
				9		
9	0					



API Units

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API Units

07JRM008 Fritz Creek, Kachemak Bay N59.6962 W151.30368 Beluga Formation

Beluga Formation								
Gamma Log	Meters	Measured Section	Facies	Facie: Assoc	Key Features	Interpretations		
			Sm					
	30 -							
	29 -							
			Sm					
90								

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Gamma Log	leters	Measured Section	acies	acies ssoc.	Key Features	Interpretations
	2			Ľ∢		
	20					
	30 -					
			Coal Fmb?	6		
	29 -		Coal			
0						



Gamma Log	ters	Measured Section	cies	cies soc.	Kev Features	Interpretations
	ĕ		- La	Fa As		
	10					
	10 -		Coal			
	15 -					
			Sm			
g	0		1			



07JRM014 Falls Creek, Kachemak Bay N59.77366 W151.12004 Sterling Formation					
Gamma Log	Meters				

Gamma Log	aters	Measured Section	Icies	acies ssoc.	Key Features	Interpretations
	≚		Fa	Fe As		
	16 -					
	15 -					
	l l	//	Sm	9?		
	/	\mathbf{X}				
	90		1	1		







Gamma Log	Meters	Measured Section	Facies	Facies Assoc.	Key Features	Interpretations
	13-		St			
	12-		Gm			
	11-		Gh			
	10 -		Sm & St			
	9-			3?		Possible inter- stratified gravelly braided fluvial and
	8-		Gm & Gh			sheetflood-domina alluvial fan deposit
	7-		Sm & St			
	6 -		Gm & Gh			
	5-					
	4 -					
	3-			3?		
	2-		Gm & Gh			
	1-					





0

cl-

÷ - E

sand

90

API Units



Gamma Log	eters	Measured Section	acies	acies ssoc.	Key Features	Interpretations
	<u></u> 69-		Gh	μų		
	68-			3?		
	67 -					
	65-		Gh			
	64 -					
	63-					
	62-		Fssl	6		Lacustrine deposits on intra or interfan low.
	60-					
	59-					
	58-					
9	57-		Gh	3?		





р С Р -

st- d

sand

API Units





Commolog	ers	Moscurad Section	ies	ies oc.	Kay Fasturas	Interpretations
Gamina Log	Met	Medsured Section	Fac	Fac Ass	Rey realures	Interpretationa
	48-		Em/2			
			F1111 ?			
	47 -			6		
			Coal			
	46		Cost			
	40-		Cool			
			Coar			
	45-					
	//	///				
	44-		Sp &			
			Sh			
				4		
		~~~				
	43-					
~						
9	ч					





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# SEDIMENTOLOGY OF AN OLIGOCENE-MIOCENE INCISED PALEOVALLEY, TYONEK FORMATION, COOK INLET BASIN, ALASKA

by

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#### **INTRODUCTION**

The Cenozoic Cook Inlet basin is located in the forearc region of the Aleutian–Alaska Peninsula magmatic arc associated with subduction of the Pacific plate beneath the North American plate (fig. 1). A complicated stratigraphy, in part due to the fluvial nature of the depositional systems, was created in the basin by cycles of uplift, denudation, and accommodation related to subduction (Swenson, 1997). Cenozoic depositional systems filled the basin with sediment eroding locally from the exposed accretionary prism to the southeast and the active volcanic arc and southern Alaska Range to the northwest (Crick, 1971; Hartman and others, 1974; Hayes and others, 1976; Hite, 1976; Swenson, 1997). Axial fluvial systems deposited material in the Cook Inlet basin that was transported from eastern Alaska and possibly as far as western Canada (Kirschner and Lyon, 1973; Rawlinson, 1984). The Paleogene and Neogene section is up to 8,500 m thick, but thins dramatically toward the basin margins (Crick, 1971).

The term "Kenai Group" was first applied to the coal-bearing exposures around Cook Inlet (Dall and Harris, 1892). Subsequently, Paleogene and Neogene sedimentary rocks on the Kenai Peninsula were designated the Kenai Formation based on multiple measured sections onshore (Barnes and Cobb, 1959), and were later elevated to group status containing five formations based on subsurface type sections (Calderwood and Fackler, 1972). The Upper Oligocene–Lower Miocene Tyonek Formation is the focus of this study.

The Tyonek Formation (2,316 m) has been described in the subsurface type section in the Pan American No. 2 Tyonek State 17587 well (fig. 2) as fine- to coarse-grained massive sandstone and siltstone with coal beds up to 6.5 m thick (Crick, 1971). However, Tyonek outcrops (Magoon and others, 1976) examined in this study consist mostly of clast-supported angular conglomerate interbedded with pedogenic siltstone, fine- to medium-grained



Figure 1. Tectonic map of the southern Alaskan plate margin showing the location of Cook Inlet basin and other important features of the convergent plate margin.

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Figure 2. Geologic map of the Barabara Point area showing the location of the measured section (modified from Bradley and others, 1999).

massive and cross-stratified sandstone, and very minor coal. This may be a reflection of the different locations within the basin of the type section and measured section in this study. The section in this study is located near the basin margin; the type section probably reflects the character of the formation away from the basin margins.

#### **METHODS**

One stratigraphic section in the Tyonek Formation was measured near Homer (fig. 2). The lithology, texture, sedimentary structures, and fossil content of the strata were recorded. Samples from mudstone and siltstone were collected for x-ray diffraction (XRD) for compositional analysis and for palynological analysis to determine relative ages; sandstone samples were collected for provenance studies. All analyses are currently underway.

#### SEDIMENTOLOGY

The Tyonek Formation measured section is exposed on the southeast coast of Kachemak Bay near Barabara Point (fig. 2). The base of the Tyonek Formation there is unconformable and erosive into the underlying structurally deformed Triassic chert and greenstone. Strata of the gently north–northeast-dipping Tyonek Formation onlap onto the underlying units near the edges of the outcrop. This exposure is interpreted as part of the fill to an incised paleovalley. The lithofacies defined in table 1 have been divided into four facies associations listed in table 2 and described below.

Code	Description	Geometry at outcrop scale
Gm	Massive, clast-supported conglomerate	Tabular and Lenticular
Gp	Planar cross-stratified clast-supported conglomerate	Tabular
Sm	Massive sandstone	Lenticular
Sh	Horizontally-stratified sandstone	Lenticular
Sp	Planar cross-stratified sandstone	Tabular
St	Trough cross-stratified sandstone	Tabular
Fsb	Angular, blocky siltstone	Tabular
Fsm	Massive siltstone	Tabular

Table 1. Summary of lithofacies.

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<b>Facies Association</b> Valley-margin ephemeral debris flows	<b>Lithofacies</b> Gm, Fsb	<b>Interpretation</b> Episodic debris flows interbedded with pedogenic siltstone horizons near the margin of an incised valley
Valley-axis proximal braided streams axis	Gm, Gp, Sh,	Sheet-flow braided stream deposits developed near the
	Sm, Fsm	of an incised paleovalley
Paludal environment	Fsm, Sm	Isolated fluvial channels laterally adjacent to overbank and marsh environments interbedded with crevasse splay deposits
Distal braided streams	St, Sp	Braided streams constructing a sandy braidplain

#### Facies Association 1: Valley-margin ephemeral debris flows

*Description.* There are two primary lithofacies in this association: Massive, clast-supported conglomerate (Gm) and massive siltstone (Fsb) (fig. 3). Facies Gm has dominantly very angular clasts with few sub-rounded types (fig. 4a). The clasts are mostly pebble- (4-16 mm) to cobble-sized (1.6-25.6 cm); the mean clast size is 2.9 cm. Clast types identified in hand specimen include variously colored chert, minor quartz, and a predominance of greenstone and metasedimentary types. Individual beds of Gm average 1-2 m thick and thicken and thin laterally. Facies Gm frequently has erosive bases, some with very steep relief (fig. 4b). The lateral extent of beds of facies Gm is on the scale of 10 m.

Facies Fsb is massive, mottled, or angular blocky. Slickensided, clay-lined surfaces, organic detritus, and rooted horizons are prevalent throughout this facies. Beds of Fsb average less than 0.5 m in thickness and are lenticular laterally. Thin lenses of conglomerate are found locally.

*Interpretation.* This facies association represents alternating periods of episodic debris flows (Gm) and relatively quiescent soil formation (Fsb) near the margins of an incised paleovalley. The angularity of the clasts suggests that they have not traveled far from their source, lending credence to proximity to a valley margin. Channel axes in this part of the section indicate a general paleoflow toward the northwest or southeast direction, but northwest-directed paleoflow is more reasonable considering the present high topography created by the growing accretionary prism to the southeast was interpreted to be present during deposition of this formation (Magoon and Egbert, 1986). Upright trees appear to be progressively buried by distinct, relatively low energy sedimentation events. Steep, erosive surfaces cut by facies Gm into underlying deposits of Fsm suggest that facies Fsb had been exposed for a long enough period of time to become cohesive (fig. 4d). Mottled textures in facies Fsb are the product of root systems that churn the soil and destroy bedding. Angular, blocky textures result from the swelling and shrinking of the sediments upon wetting and drying (Retallack, 1997). Stress cutans are surfaces that are formed by compressively orienting the clays in the sediments due to swelling, and often display slickensided surfaces as a result (fig. 4c; Bridge, 2003).

#### Facies Association 2: Valley-axis braided streams

*Description.* This facies association consists of five lithofacies present in varying abundance: Massive, clastsupported conglomerate (Gm), planar cross-stratified conglomerate (Gp), horizontally-stratified sandstone (Sh), massive sandstone (Sm), and massive siltstone (Fsm) (fig. 3). Facies Gm is most common at the base of the association, has tabular geometries at the outcrop scale (fig. 5a), and is normally graded and contains imbricated clasts. The cobble-sized clasts are sub-rounded to well rounded (fig. 5b), and generally grain size decreases upsection. The mean clast size near the base of facies association 2 is 7.2 cm, and near the middle and top of the association is 4.4 cm and 4.3 cm, respectively. Minor interbeds of medium-grained horizontally-stratified sandstone (Sh) occur within facies Gm.

Planar cross-stratified conglomerate (Gp) occurs mostly at the base of the association, and bedding is tabular at the scale of the outcrop and has similar clast characteristics to facies Gm. Facies Sm is medium-grained and typically lenticular over several meters. Facies Fsm is tabular at outcrop scale and contains minor leaf fossils and coaly horizons. Average bed thickness is 1–2 m but beds thicken and thin laterally.

Interpretation. Clasts that are rounded, in combination with normal grading in facies Gm, clast imbrication, and the presence of facies Gp and Sh all suggest tractive transportation of sediment in a fluvial setting (Miall, 2000).




Figure 4. Photographs from facies association 1 valley-margin ephemeral debris-flow deposits. A. Angular clasts dominate the massive conglomerate (Gm) near the base of the section; B. The massive conglomerate (Gm) and siltstone (Fsb) display lenticular geometries in this part of the section; C. Pedogenic features such as stress cutan surfaces with slickensides are common in the siltstone (Fsb); D. The massive conglomerate (Gm) forms steep, erosive cuts into underlying siltstone (Fsb).



Figure 5. Photographs from facies association 2 valley-axis braided stream deposits. A. The massive clast-supported conglomerate (Gm) has tabular geometries in this part of the section; B. Sub-rounded to rounded clasts of chert, quartz, greenstone, and metasedimentary types dominate the massive conglomerate (Gm) in this part of the section

The tabular nature of the conglomerate beds implies sheet-like flow similar to that in modern braided systems. Imbricated clasts suggest a paleoflow direction toward the west. The overall upsection reduction in mean clast size suggests that the system is losing transport capacity as it grades into facies association 3. This facies association is interpreted as braided stream deposits that occupy the axis of a paleovalley.

## **Facies Association 3: Paludal environment**

*Description.* The two main lithofacies in this association are massive siltstone (Fsm) and massive sandstone (Sm) (fig. 3). Facies Fsm is the dominant lithofacies but the majority of it is poorly exposed due to slumping and weathering (fig. 6). It is tabular at the scale of the outcrop and trenching revealed several rooted and coaly horizons. A few beds grade from gray siltstone to red clayey siltstone to a rooted surface.

Facies Sm consists of lenticular bodies of massively-bedded fine-grained sandstone that thicken and thin laterally with thicknesses from about 5 to 20 cm. The sandstone is gray to green and appears rich in dark micas in hand specimen. One 4-m-thick bed of lithofacies Gm is present (96 m on fig. 3); clasts within are sub-rounded to well rounded and have a mean clast size of 2.9 cm.

*Interpretation.* Thick packages of facies Fsm indicate a very low energy depositional environment. Siltstones that grade upward to clayey and rooted horizons may indicate a strongly-developed soil horizon with exposure on the order of 100,000 years (Bridge, 2003). These packages, as well as other rooted and coaly horizons, suggest deposition in overbank and swamp environments. Facies Sm may be the result of floods when laterally adjacent rivers overstepped their banks and deposited coarser material on the surrounding floodplain. The presence of facies Gm indicates minor fluvial channels.



Figure 6. Aerial field photograph from the top part of the measured section showing facies associations 3 and 4. Weathering of the dominant siltstone facies (Fsm) causes poor exposure in the paludal deposits of facies association 3. Massive sandstone (Sm) forms thin, tabular bodies in this part of the section. Note the thick, light-colored sandstone of facies association 4 exposed at the top of the section. Facies association 4 can be traced to the southeast (right) along most of the top of the 0.3-km-long outcrop.



Figure 7. Photographs from facies association 4 distal sandy braided deposits. A. Facies association 4 consists of thick beds of trough cross-stratified (St) and planar cross-stratified (Sp) sandstone; B. Several-meter-scale soft-sediment deformation is common in this association. Hammer in circle for scale.

#### **Facies Association 4: Distal braided streams**

*Description.* Facies association 4 consists of two lithofacies: trough (St) and planar (Sp) cross-stratified sandstone (fig. 3). This unit is laterally extensive and could be traced across the top of nearly the entire 0.3-km-long exposure (fig. 6). Beds in this facies are 30–40 cm thick on average, but can reach up to 1 m thick (fig. 7a). Foreset thickness ranges from 5–10 cm in some of the thicker beds and 1–2 cm in the thinner beds. Large, soft sediment deformation structures deform entire beds on the scale of over a meter (fig. 7b). Organic debris occurs on foresets and bedding planes. The sandstone is dark to light tan and appears rich in white mica in hand specimen.

*Interpretation.* Facies association 4 may represent deposition in a distal fluvial environment. The sheet-like geometry of the deposit and the evidence of tractive transport (i.e., cross-stratification) suggest deposition on a sandy braid plain. Paleoflow directions measured from facies Sp and St suggest a southerly direction. The composition of this facies looks very different in hand sample from sandstone or conglomerate compositions in the underlying associations, which could indicate a different provenance for this unit. The large-scale convolute bedding may be a sign of tectonic activity, such as subduction-related earthquakes, during deposition.

## PRELIMINARY CONCLUSIONS

The Tyonek Formation exposure on the eastern coast of Kachemak Bay is interpreted as part of the fill to an incised paleovalley. Where exposed in this area, the base of the Tyonek Formation is unconformable and erosive into the underlying structurally deformed Triassic chert and greenstone. Strata of the gently north–northeast-dipping Tyonek Formation onlap onto the underlying units at the margins of the outcrop and fill a present-day topographic low adjacent to the Triassic chert and greenstone.

Facies association 1, consisting of ephemeral debris-flow deposits and pedogenic siltstone, occurs at the base of the inferred paleovalley (fig. 7). This association represents a period when episodic high-energy sedimentation punctuated a primarily low-energy environment. This environment experienced enough subaerial exposure temporally to develop soil characteristics in the siltstone (Fsb), such as stress cutans, and to become cohesive enough that steep erosive surfaces were cut down into these deposits by conglomeratic debris flows (Gm).

Facies association 2 represents the next stage in the paleovalley, when proximal braided streams dominated the system, producing massive (Gm) and planar cross-stratified (Gp) conglomerate (fig. 7). Overbank and floodplain facies are represented by the massive siltstone (Fsm), massive sandstone (Sm), and horizontally-stratified sandstone (Sh) interbeds. Facies association 2 grades upsection to the paludal environment defined by facies association 3 (fig. 7). This marsh and floodplain environment is characterized by thick units of massive siltstone (Fsm) and thin, tabular units of massive sandstone (Sm). Facies Sm may represent crevasse splay deposits associated with isolated fluvial channels represented by lenticular bodies of massive conglomerate (Gm).

Facies association 4 is anomalous in terms of its apparent provenance, lateral extent, and bedforms. Qualitative inspection of hand specimens reveals a mica-rich composition dissimilar to the greenstone- and chert-rich lithologies of the other associations. The lateral extent of facies association 4 is much greater than the others; it extends across the top of the entire exposure and is traceable for more than 0.5 km before eroding off to the south or diving into the subsurface to the north. Thick units of trough and planar cross-stratified sandstone are unique compared to the other conglomerate- and siltstone-dominated facies associations.

The development of a paleovalley during the Late Oligocene–Early Miocene may indicate uplift in the adjacent accretionary prism at that time. Tectonic uplift of the basin margin would lead to incision of streams as relative base level drops and the river systems attempt to maintain their gradient (Bridge, 2003). Uplift of the accretionary prism would also provide a source for sediments deposited in the paleovalley; the predominance of greenstone, chert, and quartz are suitable lithologies that may have been derived from the accretionary prism. If the paleovalley extends into the offshore subsurface, stratigraphic traps commonly associated with such depositional features may exist.

## **FUTURE WORK**

A major question related to all the Tertiary depositional systems in the Cook Inlet forearc basin is what the provenance for each unit is and how it changes in time and space. For example, can we see a difference in provenance between the axial and marginal fluvial systems? One way to test this is through the use of detrital zircons. Individual zircon grains will be separated from bulk samples collected from the Tyonek, Beluga, and Sterling formations. Ages for each zircon grain will be acquired through LA–MC–ICPMS (Laser Ablation–Multiple-Collection–Inductively Coupled Plasma Mass Spectrometry) U-Th-Pb geochronological analyses. These ages will be compared to published ages obtained from all around southern Alaska in an effort to determine the provenance for each formation. This will also allow a more detailed reconstruction of the depositional systems. Key sediment source areas to focus on will include the Aleutian–Alaska Peninsula volcanic arc, the Alaska Range, the Talkeetna volcanic arc, and the Chugach Mountains (accretionary prism).

In the Seldovia area, this method can be used to analyze the provenance between the unique sandstone observed at the top of the Tyonek section (facies association 4) and that of the underlying strata. Rotation of paleocurrent directions from west- to south-directed from the base to the top of the section, as well as the different sedimentological character and the qualitative discrepancy in provenance, all suggest that the sediment sources for this part of the Tyonek may have changed as it was deposited.

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## REPORT ON DAY TRIP (5/16/07) TO VISIT MESOZOIC ROCKS EXPOSED IN PORT GRAHAM AND NEAR SELDOVIA, SOUTHERN KENAI PENINSULA

by Robert B. Blodgett¹

Field work was conducted May 16, 2007. We (Dave LePain, Alaska Division of Geological & Geophysical Surveys; Rick Stanley, U.S. Geological Survey; and myself) departed on the fourth helicopter load leaving from the Ocean Shores Motel in Homer to examine the Upper Triassic in Port Graham and Lower Jurassic west of Point Naskowhak in Kachemak Bay (see fig. 1 for location of stops visited).

### Stop 1 — Blodgett station 07RB01 (=07DL005 LePain station)

Lat. 59.35529°N, Long. 151.84725°W

Small cove (bight) along southwest side of Port Graham (NE¹/₄ SE¹/₄ NE¹/₄ Sec. 31, T9S, R15W, Seldovia B-5 Quadrangle; fig. 1). Cove has small stream (with waterfall above) flowing into it. I had chosen this cove as this is where the earlier GPS coordinates of Andrew Caruther's and George Stanley's *Monotis subcircularis* locality (their **04AC41**) was indicated. In subsequent conversation, it turns out that their locality was situated in the next cove northwest along the shoreline (probably hundred or so meters away).

The exposures at 07RB01 appear to the highly faulted. The southeastern third of the outcrop consists of volcanic-rich conglomeratic sands with locally abundant limestone clasts (most are small, but are up to 1.8 m across).



Figure 1 - Map showing two outcrop locations examined on May 16, 2007. Geology from Magoon and others (1976) compilation map. Scale is provided by the 6-mile by 6-mile township-range grid covering on-shore portions of the map. Magoon and others (1976) describe map unit Trl unit is described as Upper Triassic limestone and tuff and unit Jtk as the Lower Jurassic Talkeetna Formation consisting of volcanic breccia, tuff, agglomerate, and aphanitic lava flows. See Bradley and others (1999) for more recent mapping of Mesozoic rocks on the southern Kenai Peninsula.

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Other clast types, notably volcanic and intrusive? rocks, are present. Conglomerate at the south end weathers green-gray in color. Clasts are angular to subrounded, appear to have been transported, and individual clasts are of various colors. One limestone clast contains a number of recrystallized corals or spongiomorph specimens. We collected a number of lithology samples, and also one conodont sample (07DL005B) that was examined by Andrea Krumhardt (University of Alaska Fairbanks) and found to be barren of conodonts. We observed one mold of a high-spired gastropod reminiscent of the genus *Omphaloptychia* (see fig. 2). Fossil molds are present here (a few isolated bivalve shells) and in similar rocks on the north side of the cove (in another fault block). These fossils are difficult, if not impossible, to remove. I suggest that any future paleontological work done here include making casts of these molds using latex rubber. A light-green weathering dike is also present at the south end of this exposure.

The central part of the cove (with the stream flowing over it) consists of nearly flat-lying calcareous mudstone/shale with beds ranging from 5 mm to 5 cm thick (fig. 3). Beds strike 38° and dip 14° to the northwest. No megafossils were observed on bedding planes. The contact between the mudstone/shale section and the southerly adjacent volcanic conglomerate interval is a prominent high-angle fault. The shale beds have a weak drag fold developed in them adjacent to the fault zone.

The northern part of the cove consists of volcanic conglomerate and sandstone similar to that seen at the south end of the cove. Bivalve molds are common here and one resembles *Cassianella*, suggesting a Late Triassic age. Again, these specimens are difficult to remove, so future work here should include making latex rubber molds of these impressions.

No monotid bivalves were observed here, which were so abundant at Andrew Caruther's nearby locality 04AC41 (see fig. 4). The presence of *Monotis subcircularis* and *Halobia* (of the *superba* species type) in the past was thought to indicate the presence of both Carnian (in the case of *Halobia superba*) and late Norian (in the case of *M. subcircularis*). See reports of Martin (1915, 1926) and Silberling and others (1997) for previous noted occurrences of these species on both sides of Port Graham. Silberling and others (1997) reexamined the Halobias from older USGS collections at Port Graham and determined them to represent two middle Norian age species, *H. lineata* and *H. dilitata*, rather than *H. superba*. This reassignment indicates that all Upper Triassic fossil collections from this locality can be restricted to the middle and late Norian.

The beds at this locality appear overmature in terms of oil potential.



Figure 2. Mold of a high-spired gastropod suggestive of the genus Omphaloptychia (which is rather common in Norian strata of western North America). This specimen was found in the volcanic conglomerate/sandstone interval at the southern end of exposed beds at 07RB01.



Figure 3. Thin- to medium-bedded shale/mudstone interval that forms central part of exposure of the cove at 07RB01. No visible megafossils observed in the shale.

Figure 4. Photograph showing many specimens of Monotis subcircularis within the folded argillite layers of 04AC41 (visited by Andrew Caruthers, George Stanley, and John Kelley in 2004). My original intent was to visit this locality but Caruthers indicated GPS coordinates were probably off, as it now appears they visited the next cove immediately to the northwest of where we landed by helicopter. Monotis subcircularis is a widespread index bivalve fossil for the early late Norian (late Late Triassic). This species is very widespread in the eastern Panthalassa Ocean and is reported from western North America (both in craton and adjoining accreted terranes),



the Canadian Arctic Islands, and Peru. A few occurrences also are now known from eastern Asia (i.e., the Koryak terrane of northeastern Siberia). The monotaxic mass accumulations of this species probably indicate outer shelf depths, below wave-base, in anoxic or dysaerobic conditions. This same species is also extremely abundant and dominates near the entire Norian-age section of Kamishak Formation exposed at Puale Bay on the Alaska Peninsula. The species has previously been reported from Port Graham by Martin (1915, 1926) and Silberling and others (1997).

## Stop 2 — Blodgett stations 07RB02 and 07RB03

Two stations made in Lower Jurassic volcaniclastic rocks that lie immediately east of Tertiary Kenai Group exposures (LePain station **06DL022**) along beach approximately 2.9 km west–southwest of Point Naskowhak (NE¹/₄ NE¹/₄ Sec. 35, T9S, R15W, Seldovia B-5 Quadrangle; fig. 1). Tertiary rocks appear to fill a canyon that eroded into underlying Lower Jurassic succession. The lowermost exposed part of the Lower Jurassic section is composed of volcanic flow rock with coarse crystalline fabrics (abundant glass). Most of the Jurassic section is composed of dark greenish-gray weathering coarse volcaniclastic sandstone with mudstone interbeds and conglomeratic lenses. Exposed section is at least 20 m thick. Fossils are abundant at this section, mostly belonging to the bivalve genus *Weyla* (indicative of an Early Jurassic age). A few other undetermined bivalve species are present as well as a few undetermined high-spired gastropods. Ammonites collected here indicate an early Sinemurian (Early Jurassic) age (Imlay, 1981). Hettangian-age ammonites were also recognized at nearby localities by Imlay (1981). Martin (1915, 1926) provides antiquated faunal lists for this section.

## 07RB02

Lat. 59.44346°N, Long. 151.78622°W

Near the base of sedimentary portion of Jurassic section (west of prominent head; see fig. 5 for outcrop photo). Dave LePain notes that sedimentary structures indicate some down-slope transport here. Numerous specimens of the bivalve *Weyla* are found here (figs. 6–7), probably representing the species *Weyla alata* (von Buch, 1838). Many of these are in growth position, suggesting that although the host beds are transported, they have not been displaced great distances. Beds strike N 70°E and dip 50° toward the northwest.



Figure 5. View looking northeast (upsection) from near base of exposed Lower Jurassic section at locality 07RB02.



Figure 6. Bedding surface close to locality 07RB02 showing the large bivalve Weyla (probably Weyla alata). The rounded object near the left-center is a solitary scleractinian coral (note septa).



Figure 7. Bank of thick-shelled Weyla specimens between localities 07RB02 and 07RB3. Note that both articulated and disarticulated shells are present.

#### 07RB03

Lat. 59.44381°N, Long. 151.78600°W

Fossils of abundant *Weyla* found higher in section (above 07RB02). *Weyla* is by far the most abundant fossil at this locality (fig. 8) as well as throughout the examined section. Occurs in mass accumulations, but also a few large snails observed, and several scattered solitary colonial corals (represented by at least two species). Most beds have horizontal bounding surfaces and are internally massive, but some cross-bedding is present lower in the section. Solitary corals present (figs. 9–11), but one would need a heavy hammer and sledge to recover them. Sands here are coarse grained and appear similar to equivalent age sands seen in the Lower Jurassic section at Puale Bay.

Most of the *Weyla* occurrences are in monotaxic banks (figs. 6–7), typically in sandstones and siltstone, often articulated, but some specimens are also disarticulated.

The rocks seen at these last two exposures much less altered than those seen in the Upper Triassic at 07RB1.

## ACKNOWLEDGMENTS

I gratefully acknowledge support from DGGS to visit outcrops in the Port Graham area and Dave LePain for reviewing a draft of this manuscript.



Figure 8. Cross-section of an articulated specimen of Weyla near locality 07RB03. Note angular grain shapes indicative of transport over relatively short distances from source to depositional site.



Figure 9. Solitary scleractinian coral in cross-section (note septa). Specimen found just below locality 07RB03.



Figure 10. Base of discoidal solitary scleractinian coral from locality 07RB03. Reverse side of sample has numerous impressions of the bivalve Weyla.



Figure 11. Same solitary scleractinian coral specimen as in fig. 10 (view taken inside under poor lighting)

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## MERCURY INJECTION CAPILLARY PRESSURE RESULTS FROM OUTCROP SAMPLES IN THE HOMER AREA OF COOK INLET

by Andrea Loveland¹

## **INTRODUCTION**

This chapter summarizes mercury-injection capillary pressure data for 12 outcrop samples collected from the Beluga and Sterling formations in the vicinity of Homer, Alaska, during the 2007 field season (figs. 1 and 2). All samples are tied to measured stratigraphic sections, which are presented in LePain and others (this volume). Sample numbers correspond to measured section numbers and the sample position (meters above base of section) in a measured section. For example, sample 07JRM002–3.5a was collected 3.5 meters above the base of measured section 07JRM002. Analyses were performed by PetroTech Associates, Houston, Texas.



Figure 1. Map showing the Cook Inlet area and the locations of the measured sections from which the MICP samples were collected.

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Potential seal capacity data for gas/water and oil/water systems at four different saturation levels are summarized in figures 3a–b and 4a–b, respectively. Figures 5 and 6 illustrate the potential seal capacity for gas and oil, respectively, at 7.5% seal saturation. Mercury injection capillary pressure and pore aperture curves are presented in figures 7a–20c. Sample collection sites and lithology data are summarized in table 1. The pore system and capillary properties are summarized in table 2. Oil and gas column heights are summarized in table 3. Mercury injection capillary pressure data for each sample are presented in tables 4 through 17.

## ACKNOWLEDGMENTS

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Figure 2. Simplified stratigraphic column showing Tertiary nonmarine formations in Cook Inlet basin. Vertical red bar shows stratigraphic interval where MICP samples were collected. Modified from Swenson (2002).



Figure 3a. Potential seal capacity in a gas/water system.



Figure 3b. Potential seal capacity in a gas/water system.



Figure 4a. Potential seal capacity in an oil/water system.



Figure 4b. Potential seal capacity in an oil/water system.



Figure 5. Chart of potential seal capacity at 7.5% gas saturation in seal for each sample.



Figure 6. Chart of potential seal capacity at 7.5% oil saturation in seal for each sample.



















Figure 11c. Pore aperture size for sample 07JRM006 – 18.3a.





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samples.
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Summary
Ι.
Table

Sample	Formation	Latitude (base of measured section)	Longitude (base of measured section)	Sample Description
07JRM002 – 3.5a	Beluga Formation	59.69358	-151.30280	Shale, organic-rich; black, very fissile to thinly layered;1–2 mm coaly layers
07JRM003 – 11.0a	Beluga Formation	59.69380	-151.31266	Sandstone, very fine to occasionally fine grained; medium to light gray; well compacted; common dark rock fragments; minor to moderate mica; slight to moderate matrix?; minor visible pore space
07JRM005 - 9.1a	Beluga Formation	59.69517	-151.30707	Sandstone, very fine to occasionally medium grained; clay matrix support 95%; common dark grains; gravity flow fabric
07JRM005 - 16.5	Beluga Formation	59.69522	-151.30672	Sandstone, very fine grained, silty; laminated with very-fine to fine-grained sandstone; slightly argiilaceous; medium gray; common organics and mica with random orientation
07JRM006 - 18.3a	Beluga Formation	59.69522	-151.30672	Siltstone, very argillaceous; trace very fine sand; medium gray; common coaly organic fragments; random to local alignment
07JRM008 - 26.5a	Beluga Formation	59.69620	-151.30368	Siltstone, slightly argillaceous; light to medium gray; thin organics on bedding surfaces
07JRM009 – 19.7a	Beluga Formation	59.70012	-151.29219	Siltstone, moderately sandy (very fine to fine sand), argillaceous; light to medium gray; medium to coarse sand size rounded organics; random fabric (gravity flow?)
07DL002 - 17.2a	Beluga Formation	59.65990	-151.66521	Siltstone, argiilaceous; light to medium gray; minor mica; very minor small organics (similar to 07JRM011 – 24.7a)
07DL002 – 22.0a	Beluga Formation	59.65990	-151.66521	Siltstone, slightly sandy (very fine); laminated with argillaceous siltstone; medium gray; common grain size organics; pebbly appearance
07MAW04 – 0.6	Beluga Formation	59.67557	-151.71409	Claystone, silty; medium gray; common organics (plant debris approximately 3 mm) with random orientation; siltstone present as burrow fill (?) or due to soft sediment deformation (?)
07MAW04 – 10.3	Beluga Formation	59.67557	-151.71409	Siltstone, very argillaceous to very silty claystone; medium to light gray with some iron banding: some organics; possible small root structures (outcrop?)
ST4 – 20	Sterling Formation	60.08353	-151.62886	Claystone, silty; faint, thin laminations including some siltstone; light gray
07JRM010-34.9a	Beluga Formation	59.69879	-151.29545	Claystone, silty to very silty; minor very fine sand; light gray; small burrows (?)
07JRM011 - 24.7a	Sterling Formation	59.77030	-151.12128	Siltstone (very fine silt), argillaceous; light gray/very minor small organics

Sample Depth (ft)	Porosity (%)	Kair (md)	Median Aperture	apillary Pre entry	essure at V 5%	arious Merc 7.5%	cury Saturatior 10%
07JRM002 – 3.5a	11.3	0.0141	0.0299	964	1,500	1,735	1,962
07JRM003 – 11.0a	22.9	1.07	0.3717	78	124	138	150
07JRM005 – 9.1a	20.9	0.0856	0.1242	673	970	1,023	1,065
07JRM005 – 16.5	22.1	0.494	0.3213	175	257	279	296
07JRM006 – 18.3a	22.1	0.0682	0.1013	881	1,172	1,243	1,291
07JRM008 – 26.5a	24.0	0.422	0.2900	300	400	411	423
07JRM009 – 19.7a	21.5	0.182	0.1960	430	577	600	621
07JRM010 – 34.9a	23.3	0.0901	0.1188	881	906	940	974
07JRM011 – 24.7a	34.0	0.150	0.1117	359	590	645	708
07DL002 – 17.2a	24.3	0.137	0.1452	229	381	428	470
07DL002 – 22.0a	25.0	0.171	0.1238	112	205	257	322
07MAW04 – 0.6	26.6	0.134	0.1312	673	886	917	949
07MAW04 – 10.3	23.1	0.0808	0.1095	673	960	1,040	1,092
ST4 – 20	35.7	0.215	0.1308	470	725	845	936

Table 2. Summary of pore system and capillary properties.

Permeability calculated at maximum intrusion Median aperture size is diameter in microns

				Pressure		10%	1,134	87	616	171	746	244	359	563	409	272	186	549	631	541	465
		dynes/cm //cc	g∕cc ⁺Capillary	*Capillary	eet (oil)	7.5%	1,003	80	591	161	718	238	347	543	373	247	149	530	601	488	434
		30 0.69	0.0816	0.5780	Height in fo	5%	867	72	561	149	677	231	334	524	341	220	118	512	555	419	399
	<mark>Oil</mark> Surface	Tension – Density –		height (ft) =		%0	557	45	389	101	509	173	249	509	207	132	65	389	389	272	285
ity				Pressure		10%	837	64	454	126	551	180	265	416	302	201	137	405	466	399	343
seal capac		dynes/cm g/cc		*Capillary	et (gas)	7.5%	740	59	437	119	530	175	256	401	275	183	110	391	444	361	320
nd replot s	and replot 50 0.1360 0.4267	0.4267	leight in fe	5%	640	53	414	110	500	171	246	387	252	163	87	378	410	309	294		
ll recalculate a Gas Surface Tension – Density – height (ft) =	height (ft) =	Т	%0	411	33	287	75	376	128	183	376	153	98	48	287	287	201	210			
ht Plots es in green cells wi nsity 1.016		ssure (psia)	10%	1,962	150	1,065	296	1,291	423	621	974	708	470	322	949	1,092	936	804			
			7.5%	1,735	138	1,023	279	1,243	411	600	940	645	428	257	917	1,040	845	750			
ed In Heig g any valu	d In Heig any valu water de		illary pres	5%	1,500	124	970	257	1,172	400	577	906	590	381	205	886	960	725	069		
Data Use Changinç	Assumec	(g/cc) –			Ca	%0	964	78	673	175	881	300	430	881	359	229	112	673	673	470	493
							07JRM002 - 3.5a	07JRM003 - 11.0a	07JRM005 – 9.1a	07JRM005 - 16.5	07JRM006 - 18.3a	07JRM008 - 26.5a	07JRM009 - 19.7a	07JRM010 - 34.9a	07JRM011 - 24.7a	07DL002 – 17.2a	07DL002 – 22.0a	07MAW04 - 0.6	07MAW04 - 10.3	ST4 – 20	Average

Table 3. Summary of height data.

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#### Table 4. MICP data for sample 07JRM002 - 3.5a.

-					
Sample Informat	tion				
Bulk Volume =	4.7565 cc		Porosity =	11.3% (mercury)	
Pore Volume =	0.5363 cc		Permeability =	na	
Closure = 5.86 %	%BV @ 964 psia		Median Pore Ape	erture = 0.0299 micr	ons (diameter)
o ""				1	0 / //
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter		Vvetting Phase	vvetting Phase	Change
(psia)	(microns)	вик VOI. (%)	Saturation (%)	Change (%)	per psia
164	120	0.00	100.0	0.00	0.0000
1.04	130	0.09	100.0	0.00	0.0000
1.60	119	0.14	100.0	0.00	0.0000
1.90	109	0.20	100.0	0.00	0.0000
2.10	39.2 00 0	0.20	100.0	0.00	0.0000
2.30	90.0 92.0	0.34	100.0	0.00	0.0000
2.07	03.U 75.0	0.49	100.0	0.00	0.0000
2.81	10.9	0.63	100.0	0.00	0.0000
3.08	69.3	0.76	100.0	0.00	0.0000
3.37	63.3	0.85	100.0	0.00	0.0000
3.68	58.0	1.08	100.0	0.00	0.0000
4.03	52.9	1.23	100.0	0.00	0.0000
4.41	48.4	1.33	100.0	0.00	0.0000
4.82	44.3	1.47	100.0	0.00	0.0000
5.27	40.5	1.54	100.0	0.00	0.0000
5.77	37.0	1.63	100.0	0.00	0.0000
6.31	33.8	1.79	100.0	0.00	0.0000
6.90	30.9	1.93	100.0	0.00	0.0000
7.55	28.3	2.04	100.0	0.00	0.0000
8.26	25.8	2.17	100.0	0.00	0.0000
9.04	23.6	2.28	100.0	0.00	0.0000
9.89	21.6	2.36	100.0	0.00	0.0000
10.8	19.8	2.45	100.0	0.00	0.0000
11.8	18.1	2.53	100.0	0.00	0.0000
12.9	16.5	2.62	100.0	0.00	0.0000
14.2	15.0	2.71	100.0	0.00	0.0000
15.5	13.8	2.81	100.0	0.00	0.0000
16.9	12.6	2.93	100.0	0.00	0.0000
18.5	11.5	3.13	100.0	0.00	0.0000
20.3	10.5	3.24	100.0	0.00	0.0000
22.2	9.61	3.33	100.0	0.00	0.0000
24.3	8.78	3.41	100.0	0.00	0.0000
26.6	8.02	3.52	100.0	0.00	0.0000
29.0	7.36	3.62	100.0	0.00	0.0000
31.8	6.71	3.72	100.0	0.00	0.0000
34.8	6.13	3.81	100.0	0.00	0.0000
38.0	5.61	3.92	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM002 - 3.5a

Table 4	(cont.).	MICP data	for sample	e 07.IRM002 -	3.5a.
Inoic i	00111	miner action	joi sampic	0/0101002	0.000

Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
41.6	5.13	3.99	100.0	0.00	0.0000
45.5	4.69	4.07	100.0	0.00	0.0000
49.8	4.28	4.15	100.0	0.00	0.0000
54.5	3.91	4.23	100.0	0.00	0.0000
59.6	3.58	4.27	100.0	0.00	0.0000
65.2	3.27	4.35	100.0	0.00	0.0000
71.3	2.99	4.41	100.0	0.00	0.0000
78.0	2.73	4.44	100.0	0.00	0.0000
85.3	2.50	4.49	100.0	0.00	0.0000
93.4	2.28	4.55	100.0	0.00	0.0000
102	2.09	4.60	100.0	0.00	0.0000
112	1.90	4.67	100.0	0.00	0.0000
122	1.75	4.70	100.0	0.00	0.0000
134	1.59	4.75	100.0	0.00	0.0000
146	1.46	4.78	100.0	0.00	0.0000
160	1.33	4.83	100.0	0.00	0.0000
175	1.22	4.87	100.0	0.00	0.0000
191	1.12	4.92	100.0	0.00	0.0000
209	1.02	4.97	100.0	0.00	0.0000
229	0.932	5.00	100.0	0.00	0.0000
251	0.850	5.04	100.0	0.00	0.0000
274	0.779	5.09	100.0	0.00	0.0000
300	0.711	5.14	100.0	0.00	0.0000
328	0.650	5.18	100.0	0.00	0.0000
359	0.594	5.23	100.0	0.00	0.0000
393	0.543	5.26	100.0	0.00	0.0000
430	0.496	5.31	100.0	0.00	0.0000
470	0.454	5.35	100.0	0.00	0.0000
514	0.415	5.38	100.0	0.00	0.0000
563	0.379	5.46	100.0	0.00	0.0000
615	0.347	5.52	100.0	0.00	0.0000
673	0.317	5.57	100.0	0.00	0.0000
736	0.290	5.63	100.0	0.00	0.0000
806	0.265	5.69	100.0	0.00	0.0000
881	0.242	5.77	100.0	0.00	0.0000
964	0.221	5.86	100.0	0.00	0.0000
1050	0.203	5.94	99.3	0.69	0.0080
1150	0.186	6.05	98.3	0.96	0.0096
1260	0.169	6.15	97.4	0.96	0.0088
1380	0.155	6.28	96.3	1.10	0.0092
1510	0.141	6.43	94.9	1.38	0.0106
1650	0.129	6.60	93.4	1.51	0.0108

# Mercury Injection Capillary Pressure 07JRM002 - 3.5a

### Table 4 (cont.). MICP data for sample 07JRM002 - 3.5a.

Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1810	0.1179	6.79	91.7	1.65	0.0103
1980	0.1077	7.00	89.8	1.93	0.0113
2160	0.0988	7.23	87.8	2.06	0.0115
2370	0.0900	7.51	85.3	2.48	0.0118
2590	0.0824	7.79	82.8	2.48	0.0113
2830	0.0754	8.10	80.1	2.75	0.0115
3100	0.0688	8.44	77.0	3.03	0.0112
3390	0.0629	8.76	74.1	2.89	0.0100
3710	0.0575	9.12	71.0	3.16	0.0099
4060	0.0525	9.47	67.8	3.16	0.0090
4440	0.0480	9.81	64.8	3.03	0.0080
4850	0.0440	10.13	61.9	2.89	0.0070
5310	0.0402	10.46	59.0	2.89	0.0063
5810	0.0367	10.78	56.1	2.89	0.0058
6360	0.0335	11.09	53.4	2.75	0.0050
6950	0.0307	11.38	50.8	2.61	0.0044
7610	0.0280	11.68	48.1	2.61	0.0040
8320	0.0256	11.94	45.8	2.34	0.0033
9100	0.0234	12.18	43.6	2.20	0.0028
9960	0.0214	12.43	41.4	2.20	0.0026
10900	0.0196	12.65	39.5	1.93	0.0020
11900	0.0179	12.86	37.6	1.93	0.0019
13000	0.0164	13.08	35.6	1.93	0.0018
14300	0.0149	13.29	33.7	1.93	0.0015
15600	0.0137	13.50	31.9	1.79	0.0014
17100	0.0125	13.70	30.1	1.79	0.0012
18700	0.0114	13.90	28.3	1.79	0.0011
20400	0.0105	14.08	26.7	1.65	0.0010
22300	0.0096	14.28	24.9	1.79	0.0009
24400	0.0087	14.50	23.0	1.93	0.0009
26700	0.0080	14.71	21.0	1.93	0.0008
29300	0.0073	14.93	19.1	1.93	0.0007
32000	0.0067	15.15	17.2	1.93	0.0007
35000	0.0061	15.38	15.1	2.06	0.0007
38300	0.0056	15.62	12.9	2.20	0.0007
41900	0.0051	15.87	10.7	2.20	0.0006
45800	0.0047	16.13	8.4	2.34	0.0006
50100	0.0043	16.46	5.5	2.89	0.0007
54800	0.0039	16.76	2.8	2.75	0.0006
59500	0.0036	17.07	0.0	2.75	0.0006

# Mercury Injection Capillary Pressure 07JRM002 - 3.5a

Table 5. MICP data for sample 07JRM003 - 11.0a.

Sample Information					
Bulk Volume =	4.8422 cc		Porosity =	22.9% (mercury)	
Pore Volume =	1.1077 cc		Permeability =	1.072 md (mercury)	
Closure = 0.97 %BV @ 7	78.0 psia		Median Pore Aperture	<u>e = 0.3717 microns (dia</u>	imeter)
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	<u>per psia</u>
1.64	130	0.02	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.04	100.0	0.00	0.0000
2.15	99.2	0.06	100.0	0.00	0.0000
2.35	90.8	0.06	100.0	0.00	0.0000
2.57	83.0	0.08	100.0	0.00	0.0000
2.81	75.9	0.08	100.0	0.00	0.0000
3.08	69.3	0.10	100.0	0.00	0.0000
3.37	63.3	0.10	100.0	0.00	0.0000
3.68	58.0	0.12	100.0	0.00	0.0000
4.03	52.9	0.12	100.0	0.00	0.0000
4.41	48.4	0.14	100.0	0.00	0.0000
4.82	44.3	0.14	100.0	0.00	0.0000
5.27	40.5	0.14	100.0	0.00	0.0000
5.77	37.0	0.17	100.0	0.00	0.0000
6.31	33.8	0.17	100.0	0.00	0.0000
6.90	30.9	0.19	100.0	0.00	0.0000
7.55	28.3	0.19	100.0	0.00	0.0000
8.26	25.8	0.21	100.0	0.00	0.0000
9.04	23.6	0.21	100.0	0.00	0.0000
9.89	21.6	0.23	100.0	0.00	0.0000
10.8	19.8	0.23	100.0	0.00	0.0000
11.8	18.1	0.25	100.0	0.00	0.0000
12.9	16.5	0.27	100.0	0.00	0.0000
14.2	15.0	0.29	100.0	0.00	0.0000
15.5	13.8	0.31	100.0	0.00	0.0000
16.9	12.6	0.33	100.0	0.00	0.0000
18.5	11.5	0.35	100.0	0.00	0.0000
20.3	10.5	0.37	100.0	0.00	0.0000
22.2	9.61	0.39	100.0	0.00	0.0000
24.3	8.78	0.43	100.0	0.00	0.0000
26.6	8.02	0.45	100.0	0.00	0.0000
29.0	7.36	0.50	100.0	0.00	0.0000
31.8	6./1	0.52	100.0	0.00	0.0000
34.8	6.13	0.56	100.0	0.00	0.0000
38.0	5.61	0.60	100.0	0.00	0.0000

#### Mercury Injection Capillary Pressure 07JRM003 - 11.0a

### Table 5 (cont.). MICP data for sample 07JRM003 - 11.0a.

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	e Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
41.6	5.13	0.64	100.0	0.00	0.0000
45.5	4.69	0.68	100.0	0.00	0.0000
49.8	4.28	0.72	100.0	0.00	0.0000
54.5	3.91	0.74	100.0	0.00	0.0000
59.6	3.58	0.78	100.0	0.00	0.0000
65.2	3.27	0.83	100.0	0.00	0.0000
71.3	2.99	0.89	100.0	0.00	0.0000
78.0	2.73	0.97	100.0	0.00	0.0000
85.3	2.50	1.05	99.6	0.36	0.0495
93.4	2.28	1.20	99.0	0.63	0.0781
102	2.09	1.38	98.2	0.81	0.0945
112	1.90	1.75	96.6	1.63	0.1626
122	1.75	2.02	95.4	1.17	0.1174
134	1.59	2.50	93.3	2.08	0.1731
146	1.46	3.03	91.0	2.35	0.1957
160	1.33	3.74	87.9	3.07	0.2194
175	1.22	4.48	84.6	3.25	0.2168
191	1.12	5.29	81.1	3.52	0.2202
209	1.02	6.07	77.7	3.43	0.1907
229	0.932	6.85	74.3	3.43	0.1716
251	0.850	7.58	71.1	3.16	0.1437
274	0.779	8.18	68.5	2.62	0.1139
300	0.711	8.67	66.3	2.17	0.0834
328	0.650	9.21	64.0	2.35	0.0839
359	0.594	9.79	61.4	2.53	0.0816
393	0.543	10.32	59.1	2.35	0.0691
430	0.496	10.86	56.7	2.35	0.0635
470	0.454	11.36	54.6	2.17	0.0542
514	0.415	11.87	52.3	2.26	0.0513
563	0.379	12.28	50.5	1.81	0.0369
615	0.347	12.78	48.3	2.17	0.0417
673	0.317	13.21	46.4	1.90	0.0327
736	0.290	13.67	44.4	1.99	0.0315
806	0.265	14.10	42.5	1.90	0.0271
881	0.242	14.49	40.8	1.72	0.0229
964	0.221	14.93	38.9	1.90	0.0229
1050	0.203	15.32	37.2	1.72	0.0200
1150	0.186	15.69	35.6	1.63	0.0163
1260	0.169	16.04	34.1	1.54	0.0140
1380	0.155	16.39	32.5	1.54	0.0128
1510	0.141	16.74	31.0	1.54	0.0118
1650	0.129	17.07	29.5	1.45	0.0103

#### Mercury Injection Capillary Pressure 07JRM003 - 11.0a

## Table 5 (cont.). MICP data for sample 07JRM003 - 11.0a.

Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter		Wetting Phase	Wetting Phase	Change
(psia)	(microns)	BUIK VOI. (%)	Saturation (%)	Change (%)	per psia
1010	0.4470	17 10	00.4		
1810	0.1179	17.40	28.1	1.45	0.0090
1980	0.1077	17.69	26.8	1.26	0.0074
2160	0.0988	17.98	25.6	1.26	0.0070
2370	0.0900	18.27	24.3	1.26	0.0060
2590	0.0824	18.56	23.0	1.26	0.0057
2830	0.0754	18.81	22.0	1.08	0.0045
3100	0.0688	19.06	20.9	1.08	0.0040
3390	0.0629	19.30	19.8	1.08	0.0037
3710	0.0575	19.53	18.8	0.99	0.0031
4060	0.0525	19.76	17.8	0.99	0.0028
4440	0.0480	19.96	16.9	0.90	0.0024
4850	0.0440	20.17	16.0	0.90	0.0022
5310	0.0402	20.36	15.2	0.81	0.0018
5810	0.0367	20.54	14.4	0.81	0.0016
6360	0.0335	20.73	13.6	0.81	0.0015
6950	0.0307	20.91	12.7	0.81	0.0014
7610	0.0280	21.08	12.0	0.72	0.0011
8320	0.0256	21.24	11.3	0.72	0.0010
9100	0.0234	21.41	10.6	0.72	0.0009
9960	0.0214	21.57	9.8	0.72	0.0008
10900	0.0196	21.72	9.2	0.63	0.0007
11900	0.0179	21.86	8.6	0.63	0.0006
13000	0.0164	22.01	7.9	0.63	0.0006
14300	0.0149	22.15	7.3	0.63	0.0005
15600	0.0137	22.30	6.7	0.63	0.0005
17100	0.0125	22.42	6.1	0.54	0.0004
18700	0.0114	22.54	5.6	0.54	0.0003
20400	0.0105	22.67	5.1	0.54	0.0003
22300	0.0096	22.79	4.5	0.54	0.0003
24400	0.0087	22.92	4.0	0.54	0.0003
26700	0.0080	23.02	3.5	0.45	0.0002
29300	0.0073	23.12	3.1	0.45	0.0002
32000	0.0067	23.23	2.6	0.45	0.0002
35000	0.0061	23.33	2.2	0.45	0.0002
38300	0.0056	23.41	1.8	0.36	0.0001
41900	0.0051	23.49	1.4	0.36	0.0001
45800	0.0047	23.58	1.1	0.36	0.0001
50100	0.0043	23.64	0.8	0.27	0.0001
54800	0.0039	23.70	0.5	0.27	0.0001
59500	0.0036	23.82	0.0	0.54	0.0001

#### Mercury Injection Capillary Pressure 07JRM003 - 11.0a

#### Table 6. MICP data for sample 07JRM005 - 9.1a.

Sample Information	n				
Bulk Volume =	 8.2263 cc		Porosity =	20.9% (mercurv)	
Pore Volume -	1.7183 cc		Permeability =	0.0856 md (mercu	rv)
Closure = 1 17 %P	317 nsia		Median Pore Apertu	re = 0.1242  micron	s (diameter)
,					_ (3.3.110.01)
Capillarv	Pore Aperture	ż		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
W/	(				
1.64	130	0.02	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.04	100.0	0.00	0.0000
2.15	99.2	0.04	100.0	0.00	0.0000
2.35	90.8	0.06	100.0	0.00	0.0000
2.57	83.0	0.06	100.0	0.00	0.0000
2.81	75.9	0.06	100.0	0.00	0.0000
3.08	69.3	0.09	100.0	0.00	0.0000
3.37	63.3	0.09	100.0	0.00	0.0000
3.68	58.0	0.09	100.0	0.00	0.0000
4.03	52.9	0.09	100.0	0.00	0.0000
4.41	48.4	0.09	100.0	0.00	0.0000
4.82	44.3	0.09	100.0	0.00	0.0000
5.27	40.5	0.13	100.0	0.00	0.0000
5.77	37.0	0.13	100.0	0.00	0.0000
6.31	33.8	0.17	100.0	0.00	0.0000
6.90	30.9	0.17	100.0	0.00	0.0000
7.55	28.3	0.19	100.0	0.00	0.0000
8.26	25.8	0.19	100.0	0.00	0.0000
9.04	23.6	0.19	100.0	0.00	0.0000
9.89	21.6	0.21	100.0	0.00	0.0000
10.8	19.8	0.21	100.0	0.00	0.0000
11.8	18.1	0.23	100.0	0.00	0.0000
12.9	16.5	0.26	100.0	0.00	0.0000
14.2	15.0	0.26	100.0	0.00	0.0000
15.5	13.8	0.28	100.0	0.00	0.0000
16.9	12.6	0.28	100.0	0.00	0.0000
18.5	11.5	0.30	100.0	0.00	0.0000
20.3	10.5	0.32	100.0	0.00	0.0000
22.2	9.61	0.32	100.0	0.00	0.0000
24.3	8.78	0.34	100.0	0.00	0.0000
26.6	8.02	0.36	100.0	0.00	0.0000
29.0	7.36	0.43	100.0	0.00	0.0000
31.8	6.71	0.45	100.0	0.00	0.0000
34.8	6.13	0.47	100.0	0.00	0.0000
38.0	5.61	0.47	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM005 - 9.1a

Table 6 (cont.). MICP data for sample 07JRM005 - 9.1a.

Capillary	Pore Aperture	e		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
41.6	5.13	0.49	100.0	0.00	0.0000
45.5	4.69	0.51	100.0	0.00	0.0000
49.8	4.28	0.53	100.0	0.00	0.0000
54.5	3.91	0.53	100.0	0.00	0.0000
59.6	3.58	0.53	100.0	0.00	0.0000
65.2	3.27	0.55	100.0	0.00	0.0000
71.3	2.99	0.55	100.0	0.00	0.0000
78.0	2.73	0.58	100.0	0.00	0.0000
85.3	2.50	0.58	100.0	0.00	0.0000
93.4	2.28	0.60	100.0	0.00	0.0000
102	2.09	0.60	100.0	0.00	0.0000
112	1.90	0.62	100.0	0.00	0.0000
122	1.75	0.62	100.0	0.00	0.0000
134	1.59	0.64	100.0	0.00	0.0000
146	1.46	0.64	100.0	0.00	0.0000
160	1.33	0.66	100.0	0.00	0.0000
175	1.22	0.66	100.0	0.00	0.0000
191	1.12	0.68	100.0	0.00	0.0000
209	1.02	0.70	100.0	0.00	0.0000
229	0.932	0.72	100.0	0.00	0.0000
251	0.850	0.75	100.0	0.00	0.0000
274	0.779	0.75	100.0	0.00	0.0000
300	0.711	0.79	100.0	0.00	0.0000
328	0.650	0.81	100.0	0.00	0.0000
359	0.594	0.83	100.0	0.00	0.0000
393	0.543	0.85	100.0	0.00	0.0000
430	0.496	0.90	100.0	0.00	0.0000
470	0.454	0.94	100.0	0.00	0.0000
514	0.415	0.98	100.0	0.00	0.0000
563	0.379	1.02	100.0	0.00	0.0000
615	0.347	1.09	100.0	0.00	0.0000
673	0.317	1.17	100.0	0.00	0.0000
736	0.290	1.26	99.6	0.41	0.0065
806	0.265	1.41	98.9	0.71	0.0102
881	0.242	1.68	97.6	1.33	0.0177
964	0.221	2.15	95.3	2.24	0.0270
1050	0.203	3.01	91.2	4.08	0.0475
1150	0.186	4.65	83.4	7.86	0.0786
1260	0.169	6.42	74.9	8.47	0.0770
1380	0.155	8.23	66.2	8.67	0.0723
1510	0.141	9.95	58.0	8.27	0.0636
1650	0.129	11.17	52.1	5.82	0.0415

## Mercury Injection Capillary Pressure 07JRM005 - 9.1a

#### Table 6 (cont.). MICP data for sample 07JRM005 - 9.1a.

Capillary	Pore Aperture	Э		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1810	0.1179	12.15	47.4	4.69	0.0293
1980	0.1077	12.98	43.5	3.98	0.0234
2160	0.0988	13.68	40.1	3.37	0.0187
2370	0.0900	14.37	36.8	3.27	0.0155
2590	0.0824	14.92	34.2	2.65	0.0121
2830	0.0754	15.43	31.7	2.45	0.0102
3100	0.0688	15.90	29.5	2.24	0.0083
3390	0.0629	16.33	27.4	2.04	0.0070
3710	0.0575	16.73	25.5	1.94	0.0061
4060	0.0525	17.09	23.8	1.73	0.0050
4440	0.0480	17.44	22.1	1.63	0.0043
4850	0.0440	17.71	20.8	1.33	0.0032
5310	0.0402	18.01	19.4	1.43	0.0031
5810	0.0367	18.29	18.1	1.33	0.0027
6360	0.0335	18.54	16.8	1.22	0.0022
6950	0.0307	18.76	15.8	1.02	0.0017
7610	0.0280	18.99	14.7	1.12	0.0017
8320	0.0256	19.20	13.7	1.02	0.0014
9100	0.0234	19.44	12.6	1.12	0.0014
9960	0.0214	19.63	11.6	0.92	0.0011
10900	0.0196	19.80	10.8	0.82	0.0009
11900	0.0179	19.99	9.9	0.92	0.0009
13000	0.0164	20.16	9.1	0.82	0.0007
14300	0.0149	20.33	8.3	0.82	0.0006
15600	0.0137	20.48	7.6	0.71	0.0005
17100	0.0125	20.63	6.8	0.71	0.0005
18700	0.0114	20.78	6.1	0.71	0.0004
20400	0.0105	20.91	5.5	0.61	0.0004
22300	0.0096	21.04	4.9	0.61	0.0003
24400	0.0087	21.17	4.3	0.61	0.0003
26700	0.0080	21.27	3.8	0.51	0.0002
29300	0.0073	21.40	3.2	0.61	0.0002
32000	0.0067	21.49	2.8	0.41	0.0002
35000	0.0061	21.57	2.3	0.41	0.0001
38300	0.0056	21.68	1.8	0.51	0.0002
41900	0.0051	21.76	1.4	0.41	0.0001
45800	0.0047	21.83	1.1	0.31	0.0001
50100	0.0043	21.91	0.7	0.41	0.0001
54800	0.0039	21.98	0.4	0.31	0.0001
59500	0.0036	22.06	0.0	0.41	0.0001

# Mercury Injection Capillary Pressure 07JRM005 - 9.1a

Table 7. MICP data for sample 07JRM005 - 16.5.

Sample Informa	ation				
Bulk Volume =	5.668 cc		Porosity =	22.1% (mercury)	
Pore Volume =	1.2286 cc		Permeability =	0.494 md (mercu	ry)
Closure = 0.59	%BV @ 175 psi	а	Median Pore Apertu	ure = 0.3213 micro	ns (diameter)
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1.64	130	0.02	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2.15	99.2	0.04	100.0	0.00	0.0000
2.35	90.8	0.04	100.0	0.00	0.0000
2.57	83.0	0.06	100.0	0.00	0.0000
2.81	75.9	0.06	100.0	0.00	0.0000
3.08	69.3	0.06	100.0	0.00	0.0000
3.37	63.3	0.08	100.0	0.00	0.0000
3.68	58.0	0.08	100.0	0.00	0.0000
4.03	52.9	0.08	100.0	0.00	0.0000
4.41	48.4	0.11	100.0	0.00	0.0000
4.82	44.3	0.11	100.0	0.00	0.0000
5.27	40.5	0.11	100.0	0.00	0.0000
5.77	37.0	0.11	100.0	0.00	0.0000
6.31	33.8	0.13	100.0	0.00	0.0000
6.90	30.9	0.13	100.0	0.00	0.0000
7.55	28.3	0.13	100.0	0.00	0.0000
8.26	25.8	0.15	100.0	0.00	0.0000
9.04	23.6	0.15	100.0	0.00	0.0000
9.89	21.6	0.15	100.0	0.00	0.0000
10.8	19.8	0.15	100.0	0.00	0.0000
11.8	18.1	0.17	100.0	0.00	0.0000
12.9	16.5	0.17	100.0	0.00	0.0000
14.2	15.0	0.19	100.0	0.00	0.0000
15.5	13.8	0.19	100.0	0.00	0.0000
16.9	12.6	0.19	100.0	0.00	0.0000
18.5	11.5	0.19	100.0	0.00	0.0000
20.3	10.5	0.21	100.0	0.00	0.0000
22.2	9.61	0.21	100.0	0.00	0.0000
24.3	8.78	0.23	100.0	0.00	0.0000
26.6	8.02	0.23	100.0	0.00	0.0000
29.0	7.36	0.23	100.0	0.00	0.0000
31.8	6.71	0.25	100.0	0.00	0.0000
34.8	6.13	0.25	100.0	0.00	0.0000
38.0	5.61	0.27	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM005 - 16.5

Table 7 (cont.). MICP data for sample 07JRM005 - 16.5.

Capillary Pressure	Pore Aperture Diameter	Cumulative	Wetting Phase	Incremental Wetting Phase	Saturation Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
41.6	5.13	0.30	100.0	0.00	0.0000
45.5	4.69	0.32	100.0	0.00	0.0000
49.8	4.28	0.32	100.0	0.00	0.0000
54.5	3.91	0.32	100.0	0.00	0.0000
59.6	3.58	0.32	100.0	0.00	0.0000
65.2	3.27	0.34	100.0	0.00	0.0000
71.3	2.99	0.34	100.0	0.00	0.0000
78.0	2.73	0.36	100.0	0.00	0.0000
85.3	2.50	0.36	100.0	0.00	0.0000
93.4	2.28	0.38	100.0	0.00	0.0000
102	2.09	0.38	100.0	0.00	0.0000
112	1.90	0.40	100.0	0.00	0.0000
122	1.75	0.42	100.0	0.00	0.0000
134	1.59	0.44	100.0	0.00	0.0000
146	1.46	0.49	100.0	0.00	0.0000
160	1.33	0.53	100.0	0.00	0.0000
175	1.22	0.59	100.0	0.00	0.0000
191	1.12	0.70	99.5	0.48	0.0299
209	1.02	0.89	98.7	0.86	0.0478
229	0.932	1.18	97.3	1.34	0.0669
251	0.850	1.56	95.6	1.72	0.0782
274	0.779	2.09	93.2	2.39	0.1039
300	0.711	2.91	89.5	3.73	0.1434
328	0.650	4.20	83.7	5.83	0.2083
359	0.594	5.68	77.0	6.69	0.2159
393	0.543	6.94	71.2	5.74	0.1687
430	0.496	8.04	66.3	4.97	0.1344
470	0.454	8.97	62.0	4.21	0.1052
514	0.415	9.77	58.4	3.63	0.0826
563	0.379	10.44	55.4	3.06	0.0624
615	0.347	11.10	52.4	2.96	0.0570
673	0.317	11.71	49.6	2.77	0.0478
736	0.290	12.28	47.0	2.58	0.0410
806	0.265	12.81	44.6	2.39	0.0341
881	0.242	13.34	42.3	2.39	0.0319
964	0.221	13.88	39.8	2.49	0.0299
1050	0.203	14.41	37.4	2.39	0.0278
1150	0.186	14.81	35.6	1.82	0.0182
1260	0.169	15.17	33.9	1.63	0.0148
1380	0.155	15.55	32.2	1.72	0.0143
1510	0.141	15.91	30.6	1.63	0.0125
1650	0.129	16.25	29.1	1.53	0.0109

## Mercury Injection Capillary Pressure 07JRM005 - 16.5

Table 7 (cont.). MICP data for sample 07JRM005 - 16.5.

Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
 (psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1810	0.1179	16.58	27.5	1.53	0.0096
1980	0.1077	16.90	26.1	1.43	0.0084
2160	0.0988	17.20	24.8	1.34	0.0074
2370	0.0900	17.49	23.4	1.34	0.0064
2590	0.0824	17.77	22.2	1.24	0.0056
2830	0.0754	18.04	20.9	1.24	0.0052
3100	0.0688	18.29	19.8	1.15	0.0042
3390	0.0629	18.53	18.7	1.05	0.0036
3710	0.0575	18.76	17.7	1.05	0.0033
4060	0.0525	18.97	16.7	0.96	0.0027
4440	0.0480	19.18	15.8	0.96	0.0025
4850	0.0440	19.35	15.0	0.76	0.0019
5310	0.0402	19.54	14.1	0.86	0.0019
5810	0.0367	19.73	13.3	0.86	0.0017
6360	0.0335	19.90	12.5	0.76	0.0014
6950	0.0307	20.07	11.8	0.76	0.0013
7610	0.0280	20.23	11.0	0.76	0.0012
8320	0.0256	20.38	10.3	0.67	0.0009
9100	0.0234	20.55	9.6	0.76	0.0010
9960	0.0214	20.70	8.9	0.67	0.0008
10900	0.0196	20.85	8.2	0.67	0.0007
11900	0.0179	20.97	7.6	0.57	0.0006
13000	0.0164	21.10	7.1	0.57	0.0005
14300	0.0149	21.25	6.4	0.67	0.0005
15600	0.0137	21.37	5.8	0.57	0.0004
17100	0.0125	21.48	5.4	0.48	0.0003
18700	0.0114	21.61	4.8	0.57	0.0004
20400	0.0105	21.71	4.3	0.48	0.0003
22300	0.0096	21.82	3.8	0.48	0.0003
24400	0.0087	21.92	3.3	0.48	0.0002
26700	0.0080	22.01	3.0	0.38	0.0002
29300	0.0073	22.11	2.5	0.48	0.0002
32000	0.0067	22.20	2.1	0.38	0.0001
35000	0.0061	22.26	1.8	0.29	0.0001
38300	0.0056	22.34	1.4	0.38	0.0001
41900	0.0051	22.41	1.1	0.29	0.0001
45800	0.0047	22.47	0.9	0.29	0.0001
50100	0.0043	22.53	0.6	0.29	0.0001
54800	0.0039	22.58	0.4	0.19	0.0000
59500	0.0036	22.66	0.0	0.38	0.0001

# Mercury Injection Capillary Pressure 07JRM005 - 16.5

#### Table 8. MICP data for sample 07JRM006 - 18.3a.

Sample Information Bulk Volume =     8.2225 cc     Porosity =     22.1% (mercury)       Pore Volume =     1.8167 cc     Permeability =     0.0682 md (mercury)       Closure = 1.42 %BV @ 881 psia     Median Pore Aperture =     0.1013 microns (diameter)       Capillary Pressure     Pore Aperture Diameter     Cumulative Bulk Vol. (%)     Wetting Phase Saturation (%)     Change (%)       1.64     130     0.00     100.0     0.00     0.0000       1.86     119     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       2.81     75.9     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.08     52.9     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       4.62     44.3     0.04     100.0     0.00     0.0000 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>						
Bulk Volume =     8.2225 cc     Pores Volume =     22.1% (mercury)       Pore Volume =     1.8167 cc     Pores Volume =     0.0682 md (mercury)       Closure =     1.42 %BV @ 881 psia     Median Pore Aperture =     0.1013 microns (diameter)       Capillary Pres Aperture (microns)     Diameter Bulk Vol. (%)     Vetting Phase Wetting Phase Change (%)     Change per per sia       1.64     130     0.00     100.0     0.00     0.0000       1.80     119     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.08     58.0     0.04     100.0     0.00     0.0000       4.03     52.9     0.04     100.0     0.00     0.0000       3.04     100.0     0.00     0.0000     0.0000       4.4	Sample Informat	ion				
Pore Volume =     1.8167 cc     Permeability =     0.0682 md (mercuny)       Closure =     1.42 %BV @ 881 psia     Median Pore Aperture =     0.1013 microns (diameter)       Capillary (psia)     Pore Aperture Diameter (microns)     Cumulative Bulk Vol. (%)     Verting Phase Saturation (%)     Incremental Change (%)     Saturation per psia       1.64     130     0.00     100.0     0.00     0.0000       1.86     119     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.57     83.0     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.37     63.3     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       4.82     44.3     0.04     100.0     0.00     0.0000       4.82     44.3     0.04     100.0     0.00     0.0000       5.27     40.5     0.04	Bulk Volume =	8.2225 cc		Porosity =	22.1% (mercury)	
Closure = 1.42 %BV @ 881 psia     Median Pore Aperture = 0.1013 microns (diameter)       Capillary (psia)     Pore Aperture (microns)     Cumulative Bulk Vol. (%)     Wetting Phase Saturation (%)     Incremental Change (%)     Saturation (%)       1.64     130     0.00     100.0     0.00     0.000       1.80     119     0.02     100.0     0.00     0.000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       2.81     75.9     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.68     58.0     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       4.82     44.3     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00	Pore Volume =	1.8167 cc		Permeability =	0.0682 md (mercu	ury)
Capillary Pressure     Pore Aperture (microns)     Cumulative Bulk Vol. (%)     Wetting Phase Saturation (%)     Incremental Change (%)     Saturation per psia       1.64     130     0.00     100.0     0.00     0.000       1.80     119     0.02     100.0     0.00     0.000       2.15     99.2     0.02     100.0     0.00     0.000       2.35     90.8     0.04     100.0     0.00     0.000       2.57     83.0     0.04     100.0     0.00     0.0000       2.81     75.9     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.68     58.0     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       4.82     44.3     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0 <td>Closure = 1.42 %</td> <td>6BV @ 881 psia</td> <td>1</td> <td>Median Pore Ap</td> <td>erture = 0.1013 mi</td> <td>crons (diameter)</td>	Closure = 1.42 %	6BV @ 881 psia	1	Median Pore Ap	erture = 0.1013 mi	crons (diameter)
Capillary Pressure     Pore Aperture (microns)     Cumulative Bulk Vol. (%)     Wetting Phase Saturation (%)     Change (%) Change (%)     Saturation per psia       1.64     130     0.00     100.0     0.00     0.000       1.80     119     0.02     100.0     0.00     0.000       2.15     99.2     0.02     100.0     0.00     0.0000       2.15     99.8     0.04     100.0     0.00     0.0000       2.57     83.0     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.68     58.0     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       4.82     44.3     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0 </td <td><b>.</b></td> <td>-</td> <td></td> <td></td> <td></td> <td></td>	<b>.</b>	-				
Pressure (psia)     Diameter (microns)     Cumulative Bulk Vol. (%)     Wetting Phase Saturation (%)     Change (%) Change (%)     per psia       1.64     130     0.00     100.0     0.00     0.000       1.80     119     0.02     100.0     0.00     0.000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       2.57     83.0     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       4.03     52.9     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       5.27     40.5     0.04     100.0     0.0	Capillary	Pore Aperture	<b>A</b>		Incremental	Saturation
(psia)     (microns)     Bulk Vol. (%)     Saturation (%)     Change (%)     per psia       1.64     130     0.00     100.0     0.00     0.000       1.80     119     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       2.57     83.0     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.37     63.3     0.04     100.0     0.00     0.0000       4.03     52.9     0.04     100.0     0.00     0.0000       4.82     44.3     0.04     100.0     0.00     0.0000       5.27     40.5     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       6.31     33.8     0.07     100.0     0.00     0.0000	Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
1.64     130     0.00     100.0     0.00     0.0000       1.80     119     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       2.57     83.0     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.68     58.0     0.04     100.0     0.00     0.0000       3.68     58.0     0.04     100.0     0.00     0.0000       4.03     52.9     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       5.27     40.5     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       6.90	(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1.64     130     0.00     100.0     0.000     0.000       1.86     119     0.02     100.0     0.00     0.0000       2.15     99.2     0.02     100.0     0.00     0.0000       2.35     90.8     0.04     100.0     0.00     0.0000       2.57     83.0     0.04     100.0     0.00     0.0000       3.08     69.3     0.04     100.0     0.00     0.0000       3.37     63.3     0.04     100.0     0.00     0.0000       3.68     58.0     0.04     100.0     0.00     0.0000       4.03     52.9     0.04     100.0     0.00     0.0000       4.41     48.4     0.04     100.0     0.00     0.0000       5.27     40.5     0.04     100.0     0.00     0.0000       5.77     37.0     0.04     100.0     0.00     0.0000       6.31     33.8     0.07     100.0     0.00     0.0000       7.55	4.64	400	0.00	100.0	0.00	0.0000
1.80 $119$ $0.02$ $100.0$ $0.00$ $0.000$ $1.96$ $109$ $0.02$ $100.0$ $0.00$ $0.0000$ $2.15$ $99.2$ $0.02$ $100.0$ $0.00$ $0.0000$ $2.35$ $90.8$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.57$ $83.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.81$ $75.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.08$ $69.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.37$ $63.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.63$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.000$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.15$ $100.0$ $0.000$ $0.0000$ $9.64$ $23.6$ $0.15$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.8$ $19.8$ $0.17$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.000$ $0.0000$ <td>1.64</td> <td>130</td> <td>0.00</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	1.64	130	0.00	100.0	0.00	0.0000
1.96 $109$ $0.02$ $100.0$ $0.00$ $0.000$ $2.15$ $99.2$ $0.02$ $100.0$ $0.00$ $0.0000$ $2.35$ $90.8$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.57$ $83.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.61$ $75.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.08$ $69.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.37$ $63.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.43$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.42$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $1.29$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $1.42$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ <td>1.80</td> <td>119</td> <td>0.02</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	1.80	119	0.02	100.0	0.00	0.0000
2.15 $99.2$ $0.02$ $100.0$ $0.000$ $0.0000$ $2.35$ $90.8$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.57$ $83.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.81$ $75.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.08$ $69.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.42$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $14.3$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ <	1.96	109	0.02	100.0	0.00	0.0000
2.35 $90.8$ $0.04$ $100.0$ $0.00$ $0.000$ $2.57$ $83.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $2.81$ $75.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.08$ $69.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.37$ $63.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.44$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ <td>2.15</td> <td>99.2</td> <td>0.02</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	2.15	99.2	0.02	100.0	0.00	0.0000
2.57 $83.0$ $0.04$ $100.0$ $0.00$ $0.000$ $3.08$ $69.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.37$ $63.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.000$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.000$ $0.0000$ $14.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $14.4$ $10.5$ $0.22$ $100.0$ $0.000$ $0.0000$ $14.8$ $6.13$ $0.22$ $100.0$ $0.000$ $0.0000$ </td <td>2.35</td> <td>90.8</td> <td>0.04</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	2.35	90.8	0.04	100.0	0.00	0.0000
$2.81$ $f_{5.9}$ $0.04$ $100.0$ $0.00$ $0.000$ $3.08$ $69.3$ $0.04$ $100.0$ $0.00$ $0.000$ $3.37$ $63.3$ $0.04$ $100.0$ $0.00$ $0.000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.15$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $14.3$ $18.6$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.74$ $0.24$ $100.0$ $0.00$ $0.0000$ </td <td>2.57</td> <td>83.0</td> <td>0.04</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	2.57	83.0	0.04	100.0	0.00	0.0000
3.08 $69.3$ $0.04$ $100.0$ $0.00$ $0.000$ $3.37$ $63.3$ $0.04$ $100.0$ $0.00$ $0.000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.000$ $7.55$ $28.3$ $0.15$ $100.0$ $0.00$ $0.000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.000$ $11.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.000$ $14.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.000$ $24.3$ <td>2.81</td> <td>/5.9</td> <td>0.04</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	2.81	/5.9	0.04	100.0	0.00	0.0000
3.37 $63.3$ $0.04$ $100.0$ $0.00$ $0.000$ $3.68$ $58.0$ $0.04$ $100.0$ $0.00$ $0.000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.000$ $4.42$ $44.3$ $0.04$ $100.0$ $0.00$ $0.000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.00$ $0.000$ $15.5$ $13.8$ $0.22$ $100.0$ $0.00$ $0.000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.000$ $24.3$ <td>3.08</td> <td>69.3</td> <td>0.04</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	3.08	69.3	0.04	100.0	0.00	0.0000
3.68 $58.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.03$ $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $13.8$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ <td>3.37</td> <td>63.3</td> <td>0.04</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	3.37	63.3	0.04	100.0	0.00	0.0000
4.03 $52.9$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.41$ $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.22$ $100.0$ $0.00$ $0.0000$ $16.9$ $12.6$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.00$ $0.0000$ <	3.68	58.0	0.04	100.0	0.00	0.0000
4.41 $48.4$ $0.04$ $100.0$ $0.00$ $0.0000$ $4.82$ $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $11.5$ $0.22$ $100.0$ $0.000$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.28$ $100.0$ $0.000$ $0.0000$	4.03	52.9	0.04	100.0	0.00	0.0000
4.82 $44.3$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.27$ $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $11.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.000$ $0.0000$ $16.9$ $12.6$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$ <	4.41	48.4	0.04	100.0	0.00	0.0000
5.27 $40.5$ $0.04$ $100.0$ $0.00$ $0.0000$ $5.77$ $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.22$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $13.8$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$ <td>4.82</td> <td>44.3</td> <td>0.04</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	4.82	44.3	0.04	100.0	0.00	0.0000
5.77 $37.0$ $0.04$ $100.0$ $0.00$ $0.0000$ $6.31$ $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.000$ $0.0000$ $16.9$ $12.6$ $0.22$ $100.0$ $0.000$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0$	5.27	40.5	0.04	100.0	0.00	0.0000
6.31 $33.8$ $0.07$ $100.0$ $0.00$ $0.0000$ $6.90$ $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.00$ $0.0000$ $16.9$ $12.6$ $0.20$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $29.0$ $7.36$ $0.26$ $100.0$ $0.00$ $0.0000$ $31.8$ $6.13$ $0.28$ $100.0$ $0.00$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	5.77	37.0	0.04	100.0	0.00	0.0000
6.90 $30.9$ $0.13$ $100.0$ $0.00$ $0.0000$ $7.55$ $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.000$ $0.0000$ $16.9$ $12.6$ $0.22$ $100.0$ $0.000$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $29.0$ $7.36$ $0.26$ $100.0$ $0.000$ $0.0000$ $31.8$ $6.71$ $0.28$ $100.0$ $0.000$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	6.31	33.8	0.07	100.0	0.00	0.0000
7.55 $28.3$ $0.13$ $100.0$ $0.00$ $0.0000$ $8.26$ $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.00$ $0.0000$ $16.9$ $12.6$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.26$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.71$ $0.26$ $100.0$ $0.000$ $0.0000$ $31.8$ $6.71$ $0.26$ $100.0$ $0.000$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	6.90	30.9	0.13	100.0	0.00	0.0000
8.26 $25.8$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.04$ $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.000$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.000$ $0.0000$ $16.9$ $12.6$ $0.22$ $100.0$ $0.000$ $0.0000$ $18.5$ $11.5$ $0.22$ $100.0$ $0.000$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.000$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.000$ $0.0000$ $29.0$ $7.36$ $0.26$ $100.0$ $0.000$ $0.0000$ $31.8$ $6.71$ $0.28$ $100.0$ $0.000$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	7.55	28.3	0.13	100.0	0.00	0.0000
9.04 $23.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $9.89$ $21.6$ $0.15$ $100.0$ $0.00$ $0.0000$ $10.8$ $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.00$ $0.0000$ $16.9$ $12.6$ $0.20$ $100.0$ $0.00$ $0.0000$ $18.5$ $11.5$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $29.0$ $7.36$ $0.26$ $100.0$ $0.00$ $0.0000$ $31.8$ $6.71$ $0.28$ $100.0$ $0.00$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	8.26	25.8	0.15	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.04	23.6	0.15	100.0	0.00	0.0000
10.8 $19.8$ $0.17$ $100.0$ $0.00$ $0.0000$ $11.8$ $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.00$ $0.0000$ $16.9$ $12.6$ $0.20$ $100.0$ $0.00$ $0.0000$ $18.5$ $11.5$ $0.22$ $100.0$ $0.00$ $0.0000$ $20.3$ $10.5$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $29.0$ $7.36$ $0.26$ $100.0$ $0.00$ $0.0000$ $31.8$ $6.71$ $0.26$ $100.0$ $0.00$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	9.89	21.6	0.15	100.0	0.00	0.0000
11.8 $18.1$ $0.17$ $100.0$ $0.00$ $0.0000$ $12.9$ $16.5$ $0.17$ $100.0$ $0.00$ $0.0000$ $14.2$ $15.0$ $0.20$ $100.0$ $0.00$ $0.0000$ $15.5$ $13.8$ $0.20$ $100.0$ $0.00$ $0.0000$ $16.9$ $12.6$ $0.20$ $100.0$ $0.00$ $0.0000$ $18.5$ $11.5$ $0.22$ $100.0$ $0.00$ $0.0000$ $20.3$ $10.5$ $0.22$ $100.0$ $0.00$ $0.0000$ $22.2$ $9.61$ $0.22$ $100.0$ $0.00$ $0.0000$ $24.3$ $8.78$ $0.24$ $100.0$ $0.00$ $0.0000$ $26.6$ $8.02$ $0.24$ $100.0$ $0.00$ $0.0000$ $29.0$ $7.36$ $0.26$ $100.0$ $0.00$ $0.0000$ $31.8$ $6.71$ $0.26$ $100.0$ $0.00$ $0.0000$ $34.8$ $6.13$ $0.28$ $100.0$ $0.000$ $0.0000$	10.8	19.8	0.17	100.0	0.00	0.0000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11.8	18.1	0.17	100.0	0.00	0.0000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12.9	16.5	0.17	100.0	0.00	0.0000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14.2	15.0	0.20	100.0	0.00	0.0000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15.5	13.8	0.20	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	16.9	12.6	0.20	100.0	0.00	0.0000
20.3   10.5   0.22   100.0   0.00   0.0000     22.2   9.61   0.22   100.0   0.00   0.0000     24.3   8.78   0.24   100.0   0.00   0.0000     26.6   8.02   0.24   100.0   0.00   0.0000     29.0   7.36   0.26   100.0   0.00   0.0000     31.8   6.71   0.26   100.0   0.00   0.0000     34.8   6.13   0.28   100.0   0.00   0.0000	18.5	11.5	0.22	100.0	0.00	0.0000
22.2   9.61   0.22   100.0   0.00   0.0000     24.3   8.78   0.24   100.0   0.00   0.0000     26.6   8.02   0.24   100.0   0.00   0.0000     29.0   7.36   0.26   100.0   0.00   0.0000     31.8   6.71   0.26   100.0   0.00   0.0000     34.8   6.13   0.28   100.0   0.00   0.0000     38.0   5.61   0.28   100.0   0.00   0.0000	20.3	10.5	0.22	100.0	0.00	0.0000
24.3   8.78   0.24   100.0   0.00   0.0000     26.6   8.02   0.24   100.0   0.00   0.0000     29.0   7.36   0.26   100.0   0.00   0.0000     31.8   6.71   0.26   100.0   0.00   0.0000     34.8   6.13   0.28   100.0   0.00   0.0000     38.0   5.61   0.28   100.0   0.00   0.0000	22.2	9.61	0.22	100.0	0.00	0.0000
26.6     8.02     0.24     100.0     0.00     0.0000       29.0     7.36     0.26     100.0     0.00     0.0000       31.8     6.71     0.26     100.0     0.00     0.0000       34.8     6.13     0.28     100.0     0.00     0.0000       38.0     5.61     0.28     100.0     0.00     0.0000	24.3	8.78	0.24	100.0	0.00	0.0000
29.0   7.36   0.26   100.0   0.00   0.0000     31.8   6.71   0.26   100.0   0.00   0.0000     34.8   6.13   0.28   100.0   0.00   0.0000     38.0   5.61   0.28   100.0   0.00   0.0000	26.6	8.02	0.24	100.0	0.00	0.0000
31.8   6.71   0.26   100.0   0.00   0.0000     34.8   6.13   0.28   100.0   0.00   0.0000     38.0   5.61   0.28   100.0   0.00   0.0000	29.0	7.36	0.26	100.0	0.00	0.0000
34.8     6.13     0.28     100.0     0.00     0.0000       38.0     5.61     0.28     100.0     0.00     0.0000	31.8	6 71	0.26	100.0	0.00	0.0000
38.0 5.61 0.28 100.0 0.00 0.000	34.8	6 13	0.28	100.0	0.00	0.0000
	38.0	5.61	0.28	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM006 - 18.3a

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
41.6	5.13	0.31	100.0	0.00	0.0000
45.5	4.69	0.33	100.0	0.00	0.0000
49.8	4.28	0.33	100.0	0.00	0.0000
54.5	3.91	0.35	100.0	0.00	0.0000
59.6	3.58	0.35	100.0	0.00	0.0000
65.2	3.27	0.37	100.0	0.00	0.0000
71.3	2.99	0.37	100.0	0.00	0.0000
78.0	2.73	0.37	100.0	0.00	0.0000
85.3	2.50	0.39	100.0	0.00	0.0000
93.4	2.28	0.41	100.0	0.00	0.0000
102	2.09	0.41	100.0	0.00	0.0000
112	1.90	0.46	100.0	0.00	0.0000
122	1.75	0.48	100.0	0.00	0.0000
134	1.59	0.48	100.0	0.00	0.0000
146	1.46	0.50	100.0	0.00	0.0000
160	1.33	0.52	100.0	0.00	0.0000
175	1.22	0.59	100.0	0.00	0.0000
191	1.12	0.61	100.0	0.00	0.0000
209	1.02	0.63	100.0	0.00	0.0000
229	0.932	0.65	100.0	0.00	0.0000
251	0.850	0.68	100.0	0.00	0.0000
274	0.779	0.72	100.0	0.00	0.0000
300	0.711	0.74	100.0	0.00	0.0000
328	0.650	0.76	100.0	0.00	0.0000
359	0.594	0.81	100.0	0.00	0.0000
393	0.543	0.83	100.0	0.00	0.0000
430	0.496	0.87	100.0	0.00	0.0000
470	0.454	0.89	100.0	0.00	0.0000
514	0.415	0.94	100.0	0.00	0.0000
563	0.379	0.98	100.0	0.00	0.0000
615	0.347	1.05	100.0	0.00	0.0000
673	0.317	1.11	100.0	0.00	0.0000
736	0.290	1.20	100.0	0.00	0.0000
806	0.265	1.29	100.0	0.00	0.0000
881	0.242	1.42	100.0	0.00	0.0000
964	0.221	1.57	99.3	0.69	0.0083
1050	0.203	1.85	98.0	1.28	0.0149
1150	0.186	2.36	95.8	2.27	0.0227
1260	0.169	3.21	91.9	3.85	0.0350
1380	0.155	4.82	84.6	7.31	0.0609
1510	0.141	6.67	76.2	8.39	0.0645
1650	0.129	8.64	67.3	8.88	0.0635

## Mercury Injection Capillary Pressure 07JRM006 - 18.3a

Table 8 (cont.). MICP data for sample 07JRM006 - 18.3a.

## Table 8 (cont.). MICP data for sample 07JRM006 - 18.3a.

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
	· · · · ·			<u> </u>	I
1810	0.1179	10.32	59.7	7.60	0.0475
1980	0.1077	11.67	53.6	6.12	0.0360
2160	0.0988	12.78	48.6	5.03	0.0280
2370	0.0900	13.85	43.7	4.84	0.0230
2590	0.0824	14.72	39.8	3.95	0.0179
2830	0.0754	15.49	36.3	3.46	0.0144
3100	0.0688	16.21	33.1	3.26	0.0121
3390	0.0629	16.82	30.3	2.76	0.0095
3710	0.0575	17.36	27.8	2.47	0.0077
4060	0.0525	17.84	25.7	2.17	0.0062
4440	0.0480	18.30	23.6	2.07	0.0055
4850	0.0440	18.67	21.9	1.68	0.0041
5310	0.0402	19.04	20.2	1.68	0.0036
5810	0.0367	19.37	18.8	1.48	0.0030
6360	0.0335	19.67	17.4	1.38	0.0025
6950	0.0307	19.98	16.0	1.38	0.0023
7610	0.0280	20.24	14.8	1.18	0.0018
8320	0.0256	20.48	13.7	1.09	0.0015
9100	0.0234	20.72	12.6	1.09	0.0014
9960	0.0214	20.94	11.6	0.99	0.0011
10900	0.0196	21.13	10.8	0.89	0.0009
11900	0.0179	21.33	9.9	0.89	0.0009
13000	0.0164	21.51	9.1	0.79	0.0007
14300	0.0149	21.68	8.3	0.79	0.0006
15600	0.0137	21.83	7.6	0.69	0.0005
17100	0.0125	21.99	6.9	0.69	0.0005
18700	0.0114	22.14	6.2	0.69	0.0004
20400	0.0105	22.27	5.6	0.59	0.0003
22300	0.0096	22.40	5.0	0.59	0.0003
24400	0.0087	22.53	4.4	0.59	0.0003
26700	0.0080	22.66	3.8	0.59	0.0003
29300	0.0073	22.77	3.4	0.49	0.0002
32000	0.0067	22.88	2.9	0.49	0.0002
35000	0.0061	22.97	2.5	0.39	0.0001
38300	0.0056	23.08	2.0	0.49	0.0001
41900	0.0051	23.16	1.6	0.39	0.0001
45800	0.0047	23.25	1.2	0.39	0.0001
50100	0.0043	23.32	0.9	0.30	0.0001
54800	0.0039	23.42	0.4	0.49	0.0001
59500	0.0036	23.51	0.0	0.39	0.0001

# Mercury Injection Capillary Pressure 07JRM006 - 18.3a

Table 9. MICP data for sample 07JRM008 - 26.5a.

Sample Informat	ion				
Bulk Volume =	7.0014 cc		Porosity =	24.0% (mercury)	
Pore Volume =	1.6765 cc		Permeability =	0.422 md (mercur	y)
Closure = 0.70 %	6BV @ 300 psia		Median Pore Ap	perture = 0.290 mic	crons (diameter)
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1.04	100	0.00	100.0	0.00	0.0000
1.04	130	0.02	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2.15	99.2	0.02	100.0	0.00	0.0000
2.35	90.8	0.04	100.0	0.00	0.0000
2.57	83.0	0.04	100.0	0.00	0.0000
2.81	75.9	0.04	100.0	0.00	0.0000
3.08	69.3	0.06	100.0	0.00	0.0000
3.37	63.3	0.06	100.0	0.00	0.0000
3.68	58.0	0.06	100.0	0.00	0.0000
4.03	52.9	0.08	100.0	0.00	0.0000
4.41	48.4	0.08	100.0	0.00	0.0000
4.82	44.3	0.08	100.0	0.00	0.0000
5.27	40.5	0.10	100.0	0.00	0.0000
5.77	37.0	0.10	100.0	0.00	0.0000
6.31	33.8	0.10	100.0	0.00	0.0000
6.90	30.9	0.12	100.0	0.00	0.0000
7.55	28.3	0.12	100.0	0.00	0.0000
8.26	25.8	0.12	100.0	0.00	0.0000
9.04	23.6	0.14	100.0	0.00	0.0000
9.89	21.6	0.14	100.0	0.00	0.0000
10.8	19.8	0.16	100.0	0.00	0.0000
11.8	18.1	0.16	100.0	0.00	0.0000
12.9	16.5	0.16	100.0	0.00	0.0000
14.2	15.0	0.18	100.0	0.00	0.0000
15.5	13.8	0.18	100.0	0.00	0.0000
16.9	12.6	0.20	100.0	0.00	0.0000
18.5	11.5	0.20	100.0	0.00	0.0000
20.3	10.5	0.22	100.0	0.00	0.0000
22.2	9.61	0.22	100.0	0.00	0.0000
24.3	8.78	0.25	100.0	0.00	0.0000
26.6	8.02	0.25	100.0	0.00	0.0000
29.0	7.36	0.27	100.0	0.00	0.0000
31.8	6.71	0.29	100.0	0.00	0.0000
34.8	6.13	0.29	100.0	0.00	0.0000
38.0	5.61	0.31	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM008 - 26.5a

Table 9 (cont.).	MICP	data for s	ample (	07JRM008 -	- 26.5a.
		./	1		

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
	- 10				
41.6	5.13	0.31	100.0	0.00	0.0000
45.5	4.69	0.33	100.0	0.00	0.0000
49.8	4.28	0.33	100.0	0.00	0.0000
54.5	3.91	0.35	100.0	0.00	0.0000
59.6	3.58	0.35	100.0	0.00	0.0000
65.2	3.27	0.35	100.0	0.00	0.0000
71.3	2.99	0.35	100.0	0.00	0.0000
78.0	2.73	0.37	100.0	0.00	0.0000
85.3	2.50	0.37	100.0	0.00	0.0000
93.4	2.28	0.39	100.0	0.00	0.0000
102	2.09	0.39	100.0	0.00	0.0000
112	1.90	0.41	100.0	0.00	0.0000
122	1.75	0.43	100.0	0.00	0.0000
134	1.59	0.43	100.0	0.00	0.0000
146	1.46	0.45	100.0	0.00	0.0000
160	1.33	0.47	100.0	0.00	0.0000
175	1.22	0.49	100.0	0.00	0.0000
191	1.12	0.51	100.0	0.00	0.0000
209	1.02	0.53	100.0	0.00	0.0000
229	0.932	0.55	100.0	0.00	0.0000
251	0.850	0.59	100.0	0.00	0.0000
274	0.779	0.63	100.0	0.00	0.0000
300	0.711	0.70	100.0	0.00	0.0000
328	0.650	0.80	99.6	0.43	0.0152
359	0.594	0.98	98.8	0.77	0.0248
393	0.543	1.55	96.4	2.39	0.0703
430	0.496	3.46	88.5	7.94	0.2146
470	0.454	6.05	77.6	10.85	0.2711
514	0.415	7.89	69.9	7.69	0.1747
563	0.379	9.39	63.7	6.23	0.1272
615	0.347	10.61	58.6	5.12	0.0985
673	0.317	11.70	54.1	4.53	0.0780
736	0.290	12.68	50.0	4.10	0.0651
806	0.265	13.56	46.3	3.67	0.0525
881	0.242	14.38	42.9	3.42	0.0455
964	0.221	15.15	39.6	3.25	0.0391
1050	0.203	15.83	36.8	2.82	0.0328
1150	0.186	16.52	33.9	2.90	0.0290
1260	0.169	17.10	31.5	2.39	0.0217
1380	0.155	17.59	29.5	2.05	0.0171
1510	0.141	18.08	27.4	2.05	0.0158
1650	0.129	18.51	25.6	1.79	0.0128

## Mercury Injection Capillary Pressure 07JRM008 - 26.5a

Table 9 (cont.). MICP data for sample 07JRM008 - 26.5a.

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
1010	0.4470	10.01	<u> </u>	4 70	0.0110
1810	0.1179	18.94	23.8	1.79	0.0112
1980	0.1077	19.30	22.3	1.54	0.0090
2160	0.0988	19.65	20.8	1.45	0.0081
2370	0.0900	20.00	19.4	1.45	0.0069
2590	0.0824	20.29	18.2	1.20	0.0054
2830	0.0754	20.57	17.0	1.20	0.0050
3100	0.0688	20.84	15.9	1.11	0.0041
3390	0.0629	21.08	14.9	1.02	0.0035
3710	0.0575	21.33	13.8	1.02	0.0032
4060	0.0525	21.53	13.0	0.85	0.0024
4440	0.0480	21.74	12.1	0.85	0.0022
4850	0.0440	21.92	11.4	0.77	0.0019
5310	0.0402	22.08	10.7	0.68	0.0015
5810	0.0367	22.27	9.9	0.77	0.0015
6360	0.0335	22.43	9.2	0.68	0.0012
6950	0.0307	22.58	8.6	0.60	0.0010
7610	0.0280	22.72	8.0	0.60	0.0009
8320	0.0256	22.86	7.4	0.60	0.0008
9100	0.0234	22.98	6.9	0.51	0.0007
9960	0.0214	23.11	6.4	0.51	0.0006
10900	0.0196	23.23	5.9	0.51	0.0005
11900	0.0179	23.33	5.5	0.43	0.0004
13000	0.0164	23.43	5.0	0.43	0.0004
14300	0.0149	23.56	4.5	0.51	0.0004
15600	0.0137	23.64	4.2	0.34	0.0003
17100	0.0125	23.74	3.8	0.43	0.0003
18700	0.0114	23.84	3.3	0.43	0.0003
20400	0.0105	23.93	3.0	0.34	0.0002
22300	0.0096	24.01	2.6	0.34	0.0002
24400	0.0087	24.07	2.4	0.26	0.0001
26700	0.0080	24.15	2.0	0.34	0.0001
29300	0.0073	24.21	1.8	0.26	0.0001
32000	0.0067	24.27	1.5	0.26	0.0001
35000	0.0061	24.33	1.3	0.26	0.0001
38300	0.0056	24.40	1.0	0.26	0.0001
41900	0.0051	24.44	0.9	0.17	0.0000
45800	0.0047	24.50	0.6	0.26	0.0001
50100	0.0043	24.54	0.4	0.17	0.0000
54800	0.0039	24.58	0.3	0.17	0.0000
59500	0.0036	24.64	0.0	0.26	0.0001

# Mercury Injection Capillary Pressure 07JRM008 - 26.5a

#### Table 10. MICP data for sample 07JRM009 - 19.7a.

Sample Informat	ion				
Bulk Volume =	7.6051 cc		Porosity =	21.5% (mercury)	```
Pore Volume =	1.6356 cc		Permeability =	0.182 md (mercur	y)
Closure = $0.61$ %	ъвv @ 430 psia		iviedian Pore Ap	erture = 0.1960 m	icrons (diameter)
o					0 ( )
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1.04	100	0.00	100.0	0.00	0.0000
1.04	130	0.00	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2.15	99.2	0.02	100.0	0.00	0.0000
2.35	90.8	0.02	100.0	0.00	0.0000
2.57	83.0	0.02	100.0	0.00	0.0000
2.81	/5.9	0.02	100.0	0.00	0.0000
3.08	69.3	0.02	100.0	0.00	0.0000
3.37	63.3	0.04	100.0	0.00	0.0000
3.68	58.0	0.04	100.0	0.00	0.0000
4.03	52.9	0.08	100.0	0.00	0.0000
4.41	48.4	0.08	100.0	0.00	0.0000
4.82	44.3	0.11	100.0	0.00	0.0000
5.27	40.5	0.11	100.0	0.00	0.0000
5.77	37.0	0.11	100.0	0.00	0.0000
6.31	33.8	0.13	100.0	0.00	0.0000
6.90	30.9	0.13	100.0	0.00	0.0000
7.55	28.3	0.13	100.0	0.00	0.0000
8.26	25.8	0.15	100.0	0.00	0.0000
9.04	23.6	0.15	100.0	0.00	0.0000
9.89	21.6	0.15	100.0	0.00	0.0000
10.8	19.8	0.15	100.0	0.00	0.0000
11.8	18.1	0.15	100.0	0.00	0.0000
12.9	16.5	0.17	100.0	0.00	0.0000
14.2	15.0	0.17	100.0	0.00	0.0000
15.5	13.8	0.17	100.0	0.00	0.0000
16.9	12.6	0.17	100.0	0.00	0.0000
18.5	11.5	0.19	100.0	0.00	0.0000
20.3	10.5	0.19	100.0	0.00	0.0000
22.2	9.61	0.21	100.0	0.00	0.0000
24.3	8.78	0.21	100.0	0.00	0.0000
26.6	8.02	0.21	100.0	0.00	0.0000
29.0	7.36	0.23	100.0	0.00	0.0000
31.8	6.71	0.23	100.0	0.00	0.0000
34.8	6.13	0.25	100.0	0.00	0.0000
38.0	5.61	0.27	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM009 - 19.7a

Table 10 (cont.). MICP data for sample 07JRM009 - 19.7a.

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
44.0	5.40	0.00	100.0	0.00	0.0000
41.6	5.13	0.29	100.0	0.00	0.0000
45.5	4.69	0.32	100.0	0.00	0.0000
49.8	4.28	0.32	100.0	0.00	0.0000
54.5	3.91	0.32	100.0	0.00	0.0000
59.6	3.58	0.32	100.0	0.00	0.0000
65.2	3.27	0.34	100.0	0.00	0.0000
71.3	2.99	0.34	100.0	0.00	0.0000
78.0	2.73	0.34	100.0	0.00	0.0000
85.3	2.50	0.34	100.0	0.00	0.0000
93.4	2.28	0.34	100.0	0.00	0.0000
102	2.09	0.34	100.0	0.00	0.0000
112	1.90	0.36	100.0	0.00	0.0000
122	1.75	0.36	100.0	0.00	0.0000
134	1.59	0.36	100.0	0.00	0.0000
146	1.46	0.38	100.0	0.00	0.0000
160	1.33	0.38	100.0	0.00	0.0000
175	1.22	0.38	100.0	0.00	0.0000
191	1.12	0.40	100.0	0.00	0.0000
209	1.02	0.40	100.0	0.00	0.0000
229	0.932	0.42	100.0	0.00	0.0000
251	0.850	0.44	100.0	0.00	0.0000
274	0.779	0.46	100.0	0.00	0.0000
300	0.711	0.48	100.0	0.00	0.0000
328	0.650	0.51	100.0	0.00	0.0000
359	0.594	0.55	100.0	0.00	0.0000
393	0.543	0.57	100.0	0.00	0.0000
430	0.496	0.61	100.0	0.00	0.0000
470	0.454	0.67	99.7	0.29	0.0073
514	0.415	0.86	98.8	0.88	0.0200
563	0.379	1.37	96.5	2.35	0.0479
615	0.347	2.57	90.9	5.58	0.1073
673	0.317	4.40	82.4	8.51	0.1468
736	0.290	6.17	74.2	8.22	0.1305
806	0.265	7.83	66.4	7.73	0.1104
881	0.242	9.24	59.9	6.56	0.0874
964	0.221	10.21	55.4	4.50	0.0542
1050	0.203	11.03	51.6	3.82	0.0444
1150	0.186	11.85	47.7	3.82	0.0382
1260	0.169	12.63	44.1	3.62	0.0329
1380	0.155	13.30	41.0	3.13	0.0261
1510	0.141	13.91	38.2	2.84	0.0218
1650	0.129	14.44	35.7	2.45	0.0175

## Mercury Injection Capillary Pressure 07JRM009 - 19.7a

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### Table 10 (cont.). MICP data for sample 07JRM009 - 19.7a.

Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
1910	0 1170	14.00	22 E	2.25	0.01.11
1810	0.1179	14.92	33.5	2.20	0.0141
1980	0.1077	15.38	31.3	2.15	0.0127
2160	0.0988	15.80	29.4	1.90	0.0109
2370	0.0900	16.22	27.4	1.90	0.0093
2590	0.0824	16.60	25.0	1.70	0.0080
2030	0.0754	10.90	24.0	1.00	0.0069
3100	0.0688	17.32	22.3	1.00	0.0062
3390	0.0629	17.03	20.8	1.47	0.0051
3710	0.0575	17.93	19.5	1.37	0.0043
4060	0.0525	18.18	18.3	1.17	0.0034
4440	0.0480	18.46	17.0	1.27	0.0033
4850	0.0440	18.69	15.9	1.08	0.0026
5310	0.0402	18.90	15.0	0.98	0.0021
5810	0.0367	19.11	14.0	0.98	0.0020
6360	0.0335	19.30	13.1	0.88	0.0016
6950	0.0307	19.51	12.1	0.98	0.0017
7610	0.0280	19.70	11.3	0.88	0.0013
8320	0.0256	19.87	10.5	0.78	0.0011
9100	0.0234	20.03	9.7	0.78	0.0010
9960	0.0214	20.18	9.0	0.68	0.0008
10900	0.0196	20.33	8.3	0.68	0.0007
11900	0.0179	20.48	7.6	0.68	0.0007
13000	0.0164	20.60	7.0	0.59	0.0005
14300	0.0149	20.73	6.5	0.59	0.0005
15600	0.0137	20.85	5.9	0.59	0.0005
17100	0.0125	20.98	5.3	0.59	0.0004
18700	0.0114	21.09	4.8	0.49	0.0003
20400	0.0105	21.19	4.3	0.49	0.0003
22300	0.0096	21.28	3.9	0.39	0.0002
24400	0.0087	21.38	3.4	0.49	0.0002
26700	0.0080	21.49	2.9	0.49	0.0002
29300	0.0073	21.57	2.5	0.39	0.0002
32000	0.0067	21.63	2.3	0.29	0.0001
35000	0.0061	21.72	1.9	0.39	0.0001
38300	0.0056	21.78	1.6	0.29	0.0001
41900	0.0051	21.86	1.2	0.39	0.0001
45800	0.0047	21.91	1.0	0.20	0.0001
50100	0.0043	21.97	0.7	0.29	0.0001
54800	0.0039	22.05	0.3	0.39	0.0001
59500	0.0036	22.12	0.0	0.29	0.0001

# Mercury Injection Capillary Pressure 07JRM009 - 19.7a

Table 11. MICP data for sample 07JRM010 - 34.9a.

Sample Information	<u>on</u>				
Bulk Volume =	5.7696 cc		Porosity =	23.3% (mercury)	
Pore Volume =	1.3428 cc		Permeability =	0.0901 md (mercu	ry)
Closure = 0.69 %	BV @ 673 psia		Median Pore Apertu	re = 0.1188 microns	(diameter)
Capillary	Pore Aperture	0	M	Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1 6 4	400	0.00	100.0	0.00	0.0000
1.04	130	0.00	100.0	0.00	
1.80	119	0.00	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2.15	99.2	0.02	100.0	0.00	0.0000
2.35	90.8	0.02	100.0	0.00	0.0000
2.57	83.0	0.02	100.0	0.00	0.0000
2.81	/5.9	0.02	100.0	0.00	0.0000
3.08	69.3	0.02	100.0	0.00	0.0000
3.37	63.3	0.04	100.0	0.00	0.0000
3.68	58.0	0.04	100.0	0.00	0.0000
4.03	52.9	0.04	100.0	0.00	0.0000
4.41	48.4	0.04	100.0	0.00	0.0000
4.82	44.3	0.04	100.0	0.00	0.0000
5.27	40.5	0.04	100.0	0.00	0.0000
5.77	37.0	0.06	100.0	0.00	0.0000
6.31	33.8	0.06	100.0	0.00	0.0000
6.90	30.9	0.06	100.0	0.00	0.0000
7.55	28.3	0.08	100.0	0.00	0.0000
8.26	25.8	0.08	100.0	0.00	0.0000
9.04	23.6	0.10	100.0	0.00	0.0000
9.89	21.6	0.10	100.0	0.00	0.0000
10.8	19.8	0.10	100.0	0.00	0.0000
11.8	18.1	0.12	100.0	0.00	0.0000
12.9	16.5	0.12	100.0	0.00	0.0000
14.2	15.0	0.12	100.0	0.00	0.0000
15.5	13.8	0.14	100.0	0.00	0.0000
16.9	12.6	0.14	100.0	0.00	0.0000
18.5	11.5	0.16	100.0	0.00	0.0000
20.3	10.5	0.16	100.0	0.00	0.0000
22.2	9.61	0.16	100.0	0.00	0.0000
24.3	8.78	0.18	100.0	0.00	0.0000
26.6	8.02	0.18	100.0	0.00	0.0000
29.0	7.36	0.20	100.0	0.00	0.0000
31.8	6 71	0.20	100.0	0.00	0 0000
34 8	6 1 2	0.20	100.0	0.00	0.0000
38.0	5 61	0.22	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07JRM010 - 34.9a

Table 11 (cont.). MICP data for sample 07JRM010 - 34.9a.

Capillary	Pore Aperture	Э		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
······	· · ·	· ·	· ·	- · ·	
41.6	5.13	0.26	100.0	0.00	0.0000
45.5	4.69	0.28	100.0	0.00	0.0000
49.8	4.28	0.28	100.0	0.00	0.0000
54.5	3.91	0.28	100.0	0.00	0.0000
59.6	3.58	0.28	100.0	0.00	0.0000
65.2	3.27	0.28	100.0	0.00	0.0000
71.3	2.99	0.28	100.0	0.00	0.0000
78.0	2.73	0.30	100.0	0.00	0.0000
85.3	2.50	0.30	100.0	0.00	0.0000
93.4	2.28	0.30	100.0	0.00	0.0000
102	2.09	0.30	100.0	0.00	0.0000
112	1.90	0.32	100.0	0.00	0,0000
122	1 75	0.32	100.0	0.00	0.0000
134	1.59	0.32	100.0	0.00	0,0000
146	1 46	0.34	100.0	0.00	0,0000
160	1.33	0.34	100.0	0.00	0,0000
175	1 22	0.34	100.0	0.00	0.0000
191	1 12	0.36	100.0	0.00	0.0000
209	1.12	0.36	100.0	0.00	0.0000
229	0.932	0.38	100.0	0.00	0.0000
251	0.850	0.38	100.0	0.00	0.0000
274	0.779	0.40	100.0	0.00	0.0000
300	0.711	0.42	100.0	0.00	0.0000
328	0.650	0.42	100.0	0.00	0.0000
359	0.000	0.42	100.0	0.00	0.0000
303	0.543	0.47	100.0	0.00	0.0000
430	0.040	0.49	100.0	0.00	0.0000
430	0.450	0.53	100.0	0.00	0.0000
470 514	0.45	0.55	100.0	0.00	0.0000
563	0.370	0.50	100.0	0.00	0.0000
615	0.347	0.63	100.0	0.00	0.0000
673	0.347	0.00	100.0	0.00	0.0000
736	0.317	0.09	00.7	0.00	0.0000
806	0.250	0.07	08.8	0.33	0.0000
991	0.203	1 42	90.0	1.01	0.0124
064	0.242	2.95	90.9	6.17	0.0233
904 1050	0.221	2.00	90.7	6.26	0.0744
1050	0.203	4.51	75.0	0.20	0.0728
1260	0.100	0.01	67.1	ฮ.40 7 82	0.0940
1200	0.109	0.33	62.1	7.00 5.04	0.0711
1500	0.155	9.00	57 7	J.04 1 12	0.0420
1010	0.141	11.00	52.6	4.40	0.0341
UCOT	0.129	11.40	0.00	4.09	0.0292

# Mercury Injection Capillary Pressure 07JRM010 - 34.9a

Table 11	(cont.). MICP	data for sample	07JRM010	- 34.9a.
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Capillary	Pore Aperture	Э		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
	· · ·	· ·	· ·	- · ·	· · ·
1810	0.1179	12.39	49.7	3.91	0.0245
1980	0.1077	13.22	46.1	3.57	0.0210
2160	0.0988	13.97	42.9	3.22	0.0179
2370	0.0900	14.70	39.7	3.13	0.0149
2590	0.0824	15.35	37.0	2.78	0.0126
2830	0.0754	15.97	34.3	2.70	0.0112
3100	0.0688	16.58	31.7	2.61	0.0097
3390	0.0629	17.13	29.3	2.35	0.0081
3710	0.0575	17.63	27.1	2.17	0.0068
4060	0.0525	18.12	25.0	2.09	0.0060
4440	0.0480	18.56	23.1	1.91	0.0050
4850	0.0440	18.93	21.6	1.57	0.0038
5310	0.0402	19.31	19.9	1.65	0.0036
5810	0.0367	19.67	18.3	1.57	0.0031
6360	0.0335	20.00	17.0	1.39	0.0025
6950	0.0307	20.30	15.7	1.30	0.0022
7610	0.0280	20.60	14.3	1.30	0.0020
8320	0.0256	20.87	13.2	1.13	0.0016
9100	0.0234	21.11	12.2	1.04	0.0013
9960	0.0214	21.33	11.2	0.96	0.0011
10900	0.0196	21.55	10.3	0.96	0.0010
11900	0.0179	21.76	9.4	0.87	0.0009
13000	0.0164	21.94	8.6	0.78	0.0007
14300	0.0149	22.12	7.8	0.78	0.0006
15600	0.0137	22.28	7.1	0.70	0.0005
17100	0.0125	22.44	6.4	0.70	0.0005
18700	0.0114	22.59	5.8	0.61	0.0004
20400	0.0105	22.73	5.2	0.61	0.0004
22300	0.0096	22.87	4.6	0.61	0.0003
24400	0.0087	22.99	4.1	0.52	0.0002
26700	0.0080	23.11	3.6	0.52	0.0002
29300	0.0073	23.23	3.0	0.52	0.0002
32000	0.0067	23.33	2.6	0.43	0.0002
35000	0.0061	23.43	2.2	0.43	0.0001
38300	0.0056	23.54	1.7	0.43	0.0001
41900	0.0051	23.62	1.4	0.35	0.0001
45800	0.0047	23.70	1.0	0.35	0.0001
50100	0.0043	23.78	0.7	0.35	0.0001
54800	0.0039	23.84	0.4	0.26	0.0001
59500	0.0036	23.94	0.0	0.43	0.0001

# Mercury Injection Capillary Pressure 07JRM010 - 34.9a

### Table 12. MICP data for sample 07JRM011 - 24.7a.

Sample Information							
Bulk Volume =	 8.1398 cc		Porosity =	34.0% (mercurv)			
Pore Volume =	2.7671 cc		Permeability =	0.150 md (mercury	()		
Closure = 0.44 %	BV @ 359 psia		Median Pore Apertur	e = 0.1117 microns (	diameter)		
					,		
Capillary	Pore Aperture	!		Incremental	Saturation		
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change		
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia		
1.64	130	0.00	100.0	0.00	0.0000		
1.80	119	0.02	100.0	0.00	0.0000		
1.96	109	0.02	100.0	0.00	0.0000		
2.15	99.2	0.02	100.0	0.00	0.0000		
2.35	90.8	0.04	100.0	0.00	0.0000		
2.57	83.0	0.04	100.0	0.00	0.0000		
2.81	75.9	0.04	100.0	0.00	0.0000		
3.08	69.3	0.04	100.0	0.00	0.0000		
3.37	63.3	0.04	100.0	0.00	0.0000		
3.68	58.0	0.04	100.0	0.00	0.0000		
4.03	52.9	0.06	100.0	0.00	0.0000		
4.41	48.4	0.06	100.0	0.00	0.0000		
4.82	44.3	0.06	100.0	0.00	0.0000		
5.27	40.5	0.06	100.0	0.00	0.0000		
5.77	37.0	0.06	100.0	0.00	0.0000		
6.31	33.8	0.06	100.0	0.00	0.0000		
6.90	30.9	0.06	100.0	0.00	0.0000		
7.55	28.3	0.06	100.0	0.00	0.0000		
8.26	25.8	0.06	100.0	0.00	0.0000		
9.04	23.6	0.06	100.0	0.00	0.0000		
9.89	21.6	0.06	100.0	0.00	0.0000		
10.8	19.8	0.09	100.0	0.00	0.0000		
11.8	18.1	0.11	100.0	0.00	0.0000		
12.9	16.5	0.11	100.0	0.00	0.0000		
14.2	15.0	0.11	100.0	0.00	0.0000		
15.5	13.8	0.13	100.0	0.00	0.0000		
16.9	12.6	0.13	100.0	0.00	0.0000		
18.5	11.5	0.13	100.0	0.00	0.0000		
20.3	10.5	0.13	100.0	0.00	0.0000		
22.2	9.61	0.15	100.0	0.00	0.0000		
24.3	8.78	0.15	100.0	0.00	0.0000		
26.6	8.02	0.15	100.0	0.00	0.0000		
29.0	7.36	0.17	100.0	0.00	0.0000		
31.8	6 71	0 17	100.0	0.00	0.0000		
34.8	6 13	0 19	100.0	0.00	0.0000		
38.0	5.61	0.19	100.0	0.00	0.0000		

# Mercury Injection Capillary Pressure 07JRM011 - 24.7a

Table 12 (cont.). MICP data for sample 07JRM011 - 24.7a.

	Capillary	Pore Aperture	9		Incremental	Saturation
	Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
_	(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
	41.6	5.13	0.19	100.0	0.00	0.0000
	45.5	4.69	0.21	100.0	0.00	0.0000
	49.8	4.28	0.21	100.0	0.00	0.0000
	54.5	3.91	0.21	100.0	0.00	0.0000
	59.6	3.58	0.21	100.0	0.00	0.0000
	65.2	3.27	0.23	100.0	0.00	0.0000
	71.3	2.99	0.23	100.0	0.00	0.0000
	78.0	2.73	0.23	100.0	0.00	0.0000
	85.3	2.50	0.23	100.0	0.00	0.0000
	93.4	2.28	0.23	100.0	0.00	0.0000
	102	2.09	0.23	100.0	0.00	0.0000
	112	1.90	0.25	100.0	0.00	0.0000
	122	1.75	0.25	100.0	0.00	0.0000
	134	1.59	0.25	100.0	0.00	0.0000
	146	1.46	0.27	100.0	0.00	0.0000
	160	1.33	0.27	100.0	0.00	0.0000
	175	1.22	0.27	100.0	0.00	0.0000
	191	1.12	0.28	100.0	0.00	0.0000
	209	1.02	0.28	100.0	0.00	0.0000
	229	0.932	0.30	100.0	0.00	0.0000
	251	0.850	0.30	100.0	0.00	0.0000
	274	0.779	0.32	100.0	0.00	0.0000
	300	0.711	0.34	100.0	0.00	0.0000
	328	0.650	0.38	100.0	0.00	0.0000
	359	0.594	0.44	100.0	0.00	0.0000
	393	0.543	0.51	99.8	0.22	0.0066
	430	0.496	0.64	99.4	0.39	0.0106
	470	0.454	0.83	98.8	0.56	0.0140
	514	0.415	1.19	97.8	1.06	0.0241
	563	0.379	1.63	96.5	1.28	0.0262
	615	0.347	2.60	93.6	2.85	0.0547
	673	0.317	3.32	91.5	2.12	0.0366
	736	0.290	4.24	88.8	2.73	0.0434
	806	0.265	5.08	86.3	2.46	0.0351
	881	0.242	5.91	83.9	2.46	0.0327
	964	0.221	6.90	81.0	2.90	0.0350
	1050	0.203	7.96	77.8	3.13	0.0363
	1150	0,186	9.42	73.5	4.30	0.0430
	1260	0,169	11.09	68.6	4.91	0.0446
	1380	0,155	12.79	63.6	5.02	0.0419
	1510	0,141	14.27	59.3	4.35	0.0335
	1650	0.129	15.56	55.5	3.79	0.0271

## Mercury Injection Capillary Pressure 07JRM011 - 24.7a

## Table 12 (cont.). MICP data for sample 07JRM011 - 24.7a.

Capillary	Pore Aperture	9		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1810	0.1179	16.73	52.0	3.46	0.0216
1980	0.1077	17.87	48.7	3.35	0.0197
2160	0.0988	18.95	45.5	3.18	0.0177
2370	0.0900	20.07	42.2	3.29	0.0157
2590	0.0824	21.13	39.1	3.13	0.0142
2830	0.0754	22.15	36.0	3.01	0.0126
3100	0.0688	23.14	33.1	2.90	0.0107
3390	0.0629	24.12	30.2	2.90	0.0100
3710	0.0575	25.05	27.5	2.73	0.0085
4060	0.0525	25.92	24.9	2.57	0.0073
4440	0.0480	26.76	22.5	2.46	0.0065
4850	0.0440	27.42	20.5	1.95	0.0048
5310	0.0402	28.10	18.5	2.01	0.0044
5810	0.0367	28.75	16.6	1.90	0.0038
6360	0.0335	29.22	15.2	1.40	0.0025
6950	0.0307	29.67	13.9	1.34	0.0023
7610	0.0280	30.09	12.7	1.23	0.0019
8320	0.0256	30.43	11.7	1.00	0.0014
9100	0.0234	30.75	10.7	0.95	0.0012
9960	0.0214	31.04	9.9	0.84	0.0010
10900	0.0196	31.28	9.2	0.73	0.0008
11900	0.0179	31.53	8.4	0.73	0.0007
13000	0.0164	31.74	7.8	0.61	0.0006
14300	0.0149	31.97	7.1	0.67	0.0005
15600	0.0137	32.16	6.6	0.56	0.0004
17100	0.0125	32.35	6.0	0.56	0.0004
18700	0.0114	32.52	5.5	0.50	0.0003
20400	0.0105	32.69	5.0	0.50	0.0003
22300	0.0096	32.86	4.5	0.50	0.0003
24400	0.0087	33.03	4.0	0.50	0.0002
26700	0.0080	33.18	3.6	0.45	0.0002
29300	0.0073	33.33	3.1	0.45	0.0002
32000	0.0067	33.48	2.7	0.45	0.0002
35000	0.0061	33.63	2.2	0.45	0.0001
38300	0.0056	33.77	1.8	0.39	0.0001
41900	0.0051	33.88	1.5	0.33	0.0001
45800	0.0047	34.01	1.1	0.39	0.0001
50100	0.0043	34.13	0.8	0.33	0.0001
54800	0.0039	34.24	0.4	0.33	0.0001
59500	0.0036	34.39	0.0	0.45	0.0001

# Mercury Injection Capillary Pressure 07JRM011 - 24.7a

Table 13. MICP data for sample 07DL002 - 17.2a.

Sample Informati	on				
Bulk Volume =	6.5217 cc		Porosity =	24.3% (mercury)	
Pore Volume =	1.5831 cc		Permeability =	0.137 md (mercury)	
Closure = 0.42 %	BV @ 229 psi	a	Median Pore Apert	ure = $0.1452$ microns	(diameter)
Capillary	Pore Aperture	9		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1.64	130	0.00	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2.15	99.2	0.02	100.0	0.00	0.0000
2.35	90.8	0.02	100.0	0.00	0.0000
2.57	83.0	0.04	100.0	0.00	0.0000
2.81	75.9	0.04	100.0	0.00	0.0000
3.08	69.3	0.04	100.0	0.00	0.0000
3.37	63.3	0.04	100.0	0.00	0.0000
3.68	58.0	0.04	100.0	0.00	0.0000
4.03	52.9	0.06	100.0	0.00	0.0000
4.41	48.4	0.06	100.0	0.00	0.0000
4.82	44.3	0.06	100.0	0.00	0.0000
5.27	40.5	0.06	100.0	0.00	0.0000
5.77	37.0	0.06	100.0	0.00	0.0000
6.31	33.8	0.08	100.0	0.00	0.0000
6.90	30.9	0.08	100.0	0.00	0.0000
7.55	28.3	0.08	100.0	0.00	0.0000
8.26	25.8	0.08	100.0	0.00	0.0000
9.04	23.6	0.08	100.0	0.00	0.0000
9.89	21.6	0.10	100.0	0.00	0.0000
10.8	19.8	0.10	100.0	0.00	0.0000
11.8	18.1	0.10	100.0	0.00	0.0000
12.9	16.5	0.10	100.0	0.00	0.0000
14.2	15.0	0.10	100.0	0.00	0.0000
15.5	13.8	0.12	100.0	0.00	0.0000
16.9	12.6	0.12	100.0	0.00	0.0000
18.5	11.5	0.12	100.0	0.00	0.0000
20.3	10.5	0.12	100.0	0.00	0.0000
22.2	9.61	0.14	100.0	0.00	0.0000
24.3	8.78	0.14	100.0	0.00	0.0000
26.6	8.02	0.14	100.0	0.00	0.0000
29.0	7.36	0.14	100.0	0.00	0.0000
31.8	6.71	0.16	100.0	0.00	0.0000
34.8	6.13	0.16	100.0	0.00	0.0000
38.0	5.61	0.18	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07DL002 - 17.2a

## Table 13 (cont.). MICP data for sample 07DL002 - 17.2a.

Capillary	Pore Apertur	e O sa kati s		Incremental	Saturation
Pressure	Diameter		Wetting Phase	Vvetting Phase	Change
(psia)	(microns)	Buik Vol. (%)	Saturation (%)	Change (%)	per psia
11.0	5.40	0.40	100.0	0.00	0.0000
41.6	5.13	0.18	100.0	0.00	0.0000
45.5	4.69	0.20	100.0	0.00	0.0000
49.8	4.28	0.20	100.0	0.00	0.0000
54.5	3.91	0.20	100.0	0.00	0.0000
59.6	3.58	0.20	100.0	0.00	0.0000
65.2	3.27	0.22	100.0	0.00	0.0000
71.3	2.99	0.22	100.0	0.00	0.0000
78.0	2.73	0.22	100.0	0.00	0.0000
85.3	2.50	0.22	100.0	0.00	0.0000
93.4	2.28	0.22	100.0	0.00	0.0000
102	2.09	0.24	100.0	0.00	0.0000
112	1.90	0.24	100.0	0.00	0.0000
122	1.75	0.26	100.0	0.00	0.0000
134	1.59	0.26	100.0	0.00	0.0000
146	1.46	0.26	100.0	0.00	0.0000
160	1.33	0.28	100.0	0.00	0.0000
175	1.22	0.30	100.0	0.00	0.0000
191	1.12	0.34	100.0	0.00	0.0000
209	1.02	0.38	100.0	0.00	0.0000
229	0.932	0.42	100.0	0.00	0.0000
251	0.850	0.50	99.7	0.33	0.0151
274	0.779	0.66	99.0	0.66	0.0289
300	0.711	0.81	98.4	0.58	0.0224
328	0.650	1.03	97.5	0.91	0.0326
359	0.594	1.37	96.1	1.41	0.0455
393	0.543	1.79	94.4	1.74	0.0513
430	0.496	2.27	92.4	1.99	0.0539
470	0.454	2.84	90.0	2.33	0.0581
514	0.415	3.46	87.5	2.57	0.0585
563	0.379	4.19	84.5	2.99	0.0610
615	0.347	4.95	81.3	3.16	0.0607
673	0.317	5.56	78.8	2.49	0.0430
736	0.290	6.28	75.8	2.99	0.0475
806	0.265	6.94	73.1	2 74	0.0392
881	0 242	7 69	70.0	3.07	0.0410
964	0.221	8.51	66.6	3 41	0.0410
1050	0.203	9.34	63.2	3 41	0.0396
1150	0 186	10 27	59.4	3.82	0.0382
1260	0.160	11 21	55 5	3 00	0.0355
1380	0 155	12 04	52 1	3 41	0.0284
1510	0.100	12.04	<u>4</u> 9 1	2 00	0.0204
1650	0 1 2 9	13 41	46.4	2.00	0.0200
1000	0.120	10.41	-0	2.00	0.0100

# Mercury Injection Capillary Pressure 07DL002 - 17.2a
Table 13 (cont.).	MICP data for	• sample 071	DL002 - 17.2a.
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	Capillary	Pore Apertur	е		Incremental	Saturation
	Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
	(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
_						
	1810	0.1179	14.05	43.8	2.66	0.0166
	1980	0.1077	14.65	41.3	2.49	0.0147
	2160	0.0988	15.20	39.0	2.24	0.0125
	2370	0.0900	15.76	36.7	2.33	0.0111
	2590	0.0824	16.26	34.6	2.08	0.0094
	2830	0.0754	16.73	32.7	1.91	0.0080
	3100	0.0688	17.19	30.8	1.91	0.0071
	3390	0.0629	17.61	29.1	1.74	0.0060
	3710	0.0575	17.99	27.5	1.58	0.0049
	4060	0.0525	18.38	25.9	1.58	0.0045
	4440	0.0480	18.72	24.5	1.41	0.0037
	4850	0.0440	19.00	23.3	1.16	0.0028
	5310	0.0402	19.30	22.1	1.25	0.0027
	5810	0.0367	19.60	20.8	1.25	0.0025
	6360	0.0335	19.87	19.8	1.08	0.0020
	6950	0.0307	20.13	18.7	1.08	0.0018
	7610	0.0280	20.39	17.6	1.08	0.0016
	8320	0.0256	20.63	16.6	1.00	0.0014
	9100	0.0234	20.87	15.6	1.00	0.0013
	9960	0.0214	21.11	14.6	1.00	0.0012
	10900	0.0196	21.36	13.6	1.00	0.0011
	11900	0.0179	21.60	12.6	1.00	0.0010
	13000	0.0164	21.82	11.7	0.91	0.0008
	14300	0.0149	22.08	10.6	1.08	0.0008
	15600	0.0137	22.30	9.7	0.91	0.0007
	17100	0.0125	22.52	8.8	0.91	0.0006
	18700	0.0114	22.74	7.9	0.91	0.0006
	20400	0.0105	22.95	7.1	0.83	0.0005
	22300	0.0096	23.13	6.3	0.75	0.0004
	24400	0.0087	23.31	5.6	0.75	0.0004
	26700	0.0080	23.49	4.8	0.75	0.0003
	29300	0.0073	23.65	4.2	0.66	0.0003
	32000	0.0067	23.81	3.5	0.66	0.0002
	35000	0.0061	23.95	2.9	0.58	0.0002
	38300	0.0056	24.07	2.4	0.50	0.0002
	41900	0.0051	24.19	1.9	0.50	0.0001
	45800	0.0047	24.31	1.4	0.50	0.0001
	50100	0.0043	24.44	0.9	0.50	0.0001
	54800	0.0039	24.56	0.4	0.50	0.0001
	59500	0.0036	24.66	0.0	0.42	0.0001

# Mercury Injection Capillary Pressure 07DL002 - 17.2a

### Table 14. MICP data for sample 07DL002 - 22.0a.

Sample Informati	00				
Bulk Volumo -	5 0497 cc		Porosity -	25.0% (moreury)	
Pore Volume -	1 2628 00		Pormoability –	23.0% (mercury)	
Closure = 0.71 %	RV @ 112 neia		Median Pore An	erture = $0.1238$ micro	ns (diameter)
	DV S I IZ Pola		Median Fule Ap		
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(nsia)	(microns)		Saturation (%)	Change (%)	ner nsia
(pold)	(111010113)	Baik Vol. (70)	Outdration (70)		
1 64	130	0.02	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2 15	99.2	0.04	100.0	0.00	0.0000
2.35	90.8	0.04	100.0	0.00	0.0000
2.57	83.0	0.08	100.0	0.00	0.0000
2.81	75.9	0.08	100.0	0.00	0.0000
3.08	69.3	0.10	100.0	0.00	0.0000
3.37	63.3	0.10	100.0	0.00	0.0000
3.68	58.0	0.12	100.0	0.00	0.0000
4 03	52.9	0.12	100.0	0.00	0.0000
4 41	48.4	0.12	100.0	0.00	0.0000
4 82	44.3	0.14	100.0	0.00	0.0000
5.27	40.5	0.16	100.0	0.00	0.0000
5.77	37.0	0.16	100.0	0.00	0.0000
6.31	33.8	0.18	100.0	0.00	0.0000
6.90	30.9	0.18	100.0	0.00	0.0000
7.55	28.3	0.20	100.0	0.00	0.0000
8.26	25.8	0.20	100.0	0.00	0.0000
9.04	23.6	0.20	100.0	0.00	0.0000
9.89	21.6	0.22	100.0	0.00	0.0000
10.8	19.8	0.22	100.0	0.00	0.0000
11.8	18.1	0.24	100.0	0.00	0.0000
12.9	16.5	0.24	100.0	0.00	0.0000
14.2	15.0	0.26	100.0	0.00	0.0000
15.5	13.8	0.28	100.0	0.00	0.0000
16.9	12.6	0.30	100.0	0.00	0.0000
18.5	11.5	0.30	100.0	0.00	0.0000
20.3	10.5	0.32	100.0	0.00	0.0000
22.2	9.61	0.32	100.0	0.00	0.0000
24.3	8.78	0.34	100.0	0.00	0.0000
26.6	8.02	0.36	100.0	0.00	0.0000
29.0	7.36	0.38	100.0	0.00	0.0000
31.8	6.71	0.40	100.0	0.00	0.0000
34.8	6.13	0.42	100.0	0.00	0.0000
38.0	5.61	0.42	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07DL002 - 22.0a

Table 14 (cont.	). MICP	data for	sample	07DL002 ·	· 22.0a.
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Capillary Pressure (psia)	Pore Aperture Diameter (microns)	Cumulative Bulk Vol. (%)	Wetting Phase Saturation (%)	Incremental Wetting Phase Change (%)	Saturation Change per psia
41.6	5.13	0.46	100.0	0.00	0.0000
45.5	4.69	0.48	100.0	0.00	0.0000
49.8	4.28	0.48	100.0	0.00	0.0000
54.5	3.91	0.50	100.0	0.00	0.0000
59.6	3.58	0.50	100.0	0.00	0.0000
65.2	3.27	0.52	100.0	0.00	0.0000
71.3	2.99	0.54	100.0	0.00	0.0000
78.0	2.73	0.54	100.0	0.00	0.0000
85.3	2.50	0.55	100.0	0.00	0.0000
93.4	2.28	0.59	100.0	0.00	0.0000
102	2.09	0.63	100.0	0.00	0.0000
112	1.90	0.71	100.0	0.00	0.0000
122	1.75	0.79	99.7	0.32	0.0317
134	1.59	0.91	99.2	0.48	0.0397
146	1.46	1.09	98.5	0.71	0.0595
160	1.33	1.33	97.5	0.95	0.0680
175	1.22	1.57	96.6	0.95	0.0634
191	1.12	1.78	95.7	0.87	0.0545
209	1.02	2.00	94.8	0.87	0.0485
229	0.932	2.26	93.8	1.03	0.0515
251	0.850	2.54	92.7	1.11	0.0505
274	0.779	2.79	91.7	1.03	0.0448
300	0.711	3.01	90.8	0.87	0.0336
328	0.650	3.27	89.8	1.03	0.0368
359	0.594	3.55	88.7	1.11	0.0358
393	0.543	3.81	87.6	1.03	0.0303
430	0.496	4.08	86.5	1.11	0.0300
470	0.454	4.36	85.4	1.11	0.0278
514	0.415	4.70	84.1	1.35	0.0306
563	0.379	4.99	82.9	1.19	0.0243
615	0.347	5.37	81.4	1.51	0.0290
673	0.317	5.81	79.6	1.74	0.0301
736	0.290	6.32	77.6	2.06	0.0327
806	0.265	7.02	74.8	2.78	0.0397
881	0.242	7.79	71.7	3.09	0.0412
964	0.221	8.50	68.8	2.85	0.0344
1050	0.203	9.24	65.9	2.93	0.0341
1150	0.186	10.05	62.6	3.25	0.0325
1260	0.169	10.82	59.6	3.09	0.0281
1380	0.155	11.53	56.7	2.85	0.0238
1510	0.141	12.21	54.0	2.70	0.0207
1650	0.129	12.88	51.3	2.70	0.0193

## Mercury Injection Capillary Pressure 07DL002 - 22.0a

### Table 14 (cont.). MICP data for sample 07DL002 - 22.0a.

Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Buik vol. (%)	Saturation (%)	Change (%)	per psia
1010	0 4 4 7 0	40.50	40.0	0.70	0.0400
1810	0.1179	13.56	48.6	2.70	0.0169
1980	0.1077	14.21	40.0	2.62	0.0154
2160	0.0988	14.82	43.5	2.40	0.0137
2370	0.0900	15.48	40.9	2.62	0.0125
2590	0.0824	16.09	38.5	2.46	0.0112
2830	0.0754	16.67	36.2	2.30	0.0096
3100	0.0688	17.24	33.9	2.30	0.0085
3390	0.0629	17.76	31.8	2.06	0.0071
3710	0.0575	18.25	29.8	1.98	0.0062
4060	0.0525	18.71	28.0	1.82	0.0052
4440	0.0480	19.13	26.3	1.67	0.0044
4850	0.0440	19.46	25.0	1.35	0.0033
5310	0.0402	19.82	23.6	1.43	0.0031
5810	0.0367	20.16	22.2	1.35	0.0027
6360	0.0335	20.47	20.9	1.27	0.0023
6950	0.0307	20.75	19.8	1.11	0.0019
7610	0.0280	21.03	18.7	1.11	0.0017
8320	0.0256	21.31	17.6	1.11	0.0016
9100	0.0234	21.56	16.6	1.03	0.0013
9960	0.0214	21.82	15.5	1.03	0.0012
10900	0.0196	22.08	14.5	1.03	0.0011
11900	0.0179	22.32	13.6	0.95	0.0010
13000	0.0164	22.55	12.6	0.95	0.0009
14300	0.0149	22.81	11.6	1.03	0.0008
15600	0.0137	23.05	10.6	0.95	0.0007
17100	0.0125	23.29	9.7	0.95	0.0006
18700	0.0114	23.53	8.7	0.95	0.0006
20400	0.0105	23.72	7.9	0.79	0.0005
22300	0.0096	23.94	7.1	0.87	0.0005
24400	0.0087	24.14	6.3	0.79	0.0004
26700	0.0080	24.34	5.5	0.79	0.0003
29300	0.0073	24.52	4.8	0.71	0.0003
32000	0.0067	24.67	4.1	0.63	0.0002
35000	0.0061	24.83	3.5	0.63	0.0002
38300	0.0056	24.99	2.9	0.63	0.0002
41900	0.0051	25.13	2.3	0.56	0.0002
45800	0.0047	25.27	1.7	0.56	0.0001
50100	0.0043	25.39	1.3	0.48	0.0001
54800	0.0039	25.53	0.7	0.56	0.0001
59500	0.0036	25.71	0.0	0.71	0.0002

## Mercury Injection Capillary Pressure 07DL002 - 22.0a

Table 15. MICP data for sample 07MAW04 - 0.6.

				1	
Sample Informati	ion		<b>_</b>		
Bulk Volume =	8.6502 cc		Porosity =	26.6% (mercury)	
Pore Volume =	2.2026 cc		Permeability =	0.134 md (mercury)	. / P
Closure = 0.85 %	₀в∨ @ 673 psia	1	Median Pore Ape	erture = 0.1312 microns	s (diameter)
<b>.</b>					
Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
					0.000
1.64	130	0.00	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.02	100.0	0.00	0.0000
2.15	99.2	0.02	100.0	0.00	0.0000
2.35	90.8	0.02	100.0	0.00	0.0000
2.57	83.0	0.04	100.0	0.00	0.0000
2.81	75.9	0.04	100.0	0.00	0.0000
3.08	69.3	0.04	100.0	0.00	0.0000
3.37	63.3	0.04	100.0	0.00	0.0000
3.68	58.0	0.06	100.0	0.00	0.0000
4.03	52.9	0.06	100.0	0.00	0.0000
4.41	48.4	0.06	100.0	0.00	0.0000
4.82	44.3	0.06	100.0	0.00	0.0000
5.27	40.5	0.06	100.0	0.00	0.0000
5.77	37.0	0.06	100.0	0.00	0.0000
6.31	33.8	0.06	100.0	0.00	0.0000
6.90	30.9	0.06	100.0	0.00	0.0000
7.55	28.3	0.06	100.0	0.00	0.0000
8.26	25.8	0.08	100.0	0.00	0.0000
9.04	23.6	0.08	100.0	0.00	0.0000
9.89	21.6	0.08	100.0	0.00	0.0000
10.8	19.8	0.08	100.0	0.00	0.0000
11.8	18.1	0.08	100.0	0.00	0.0000
12.9	16.5	0.08	100.0	0.00	0.0000
14.2	15.0	0.08	100.0	0.00	0.0000
15.5	13.8	0.10	100.0	0.00	0.0000
16.9	12.6	0.10	100.0	0.00	0.0000
18.5	11.5	0.10	100.0	0.00	0.0000
20.3	10.5	0.12	100.0	0.00	0.0000
22.2	9.61	0.12	100.0	0.00	0.0000
24.3	8.78	0.12	100.0	0.00	0.0000
26.6	8.02	0.14	100.0	0.00	0.0000
29.0	7.36	0.16	100.0	0.00	0.0000
31.8	6.71	0.16	100.0	0.00	0.0000
34.8	6.13	0.18	100.0	0.00	0.0000
38.0	5.61	0.18	100.0	0.00	0.0000

## Mercury Injection Capillary Pressure 07MAW04 - 0.6

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Table 15 (cont.). MICP data for sample 07MAW04 - 0.6.

Capillary	Pore Aperture	e		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
41.6	5.13	0.20	100.0	0.00	0.0000
45.5	4.69	0.24	100.0	0.00	0.0000
49.8	4.28	0.24	100.0	0.00	0.0000
54.5	3.91	0.24	100.0	0.00	0.0000
59.6	3.58	0.24	100.0	0.00	0.0000
65.2	3.27	0.24	100.0	0.00	0.0000
71.3	2.99	0.24	100.0	0.00	0.0000
78.0	2.73	0.24	100.0	0.00	0.0000
85.3	2.50	0.26	100.0	0.00	0.0000
93.4	2.28	0.26	100.0	0.00	0.0000
102	2.09	0.26	100.0	0.00	0.0000
112	1.90	0.26	100.0	0.00	0.0000
122	1.75	0.26	100.0	0.00	0.0000
134	1.59	0.26	100.0	0.00	0.0000
146	1.46	0.28	100.0	0.00	0.0000
160	1.33	0.28	100.0	0.00	0.0000
175	1.22	0.28	100.0	0.00	0.0000
191	1.12	0.29	100.0	0.00	0.0000
209	1.02	0.31	100.0	0.00	0.0000
229	0.932	0.33	100.0	0.00	0.0000
251	0.850	0.33	100.0	0.00	0.0000
274	0.779	0.35	100.0	0.00	0.0000
300	0.711	0.37	100.0	0.00	0.0000
328	0.650	0.37	100.0	0.00	0.0000
359	0.594	0.41	100.0	0.00	0.0000
393	0.543	0.43	100.0	0.00	0.0000
430	0.496	0.47	100.0	0.00	0.0000
470	0.454	0.51	100.0	0.00	0.0000
514	0.415	0.55	100.0	0.00	0.0000
563	0.379	0.63	100.0	0.00	0.0000
615	0.347	0.71	100.0	0.00	0.0000
673	0.317	0.85	100.0	0.00	0.0000
736	0.290	1.08	99.1	0.89	0.0141
806	0.265	1.44	97.8	1.33	0.0190
881	0.242	2.06	95.4	2.36	0.0315
964	0.221	3.83	88.8	6.65	0.0801
1050	0.203	5.88	81.1	7.68	0.0893
1150	0.186	8.61	70.8	10.27	0.1027
1260	0.169	10.52	63.7	7.16	0.0651
1380	0.155	12.05	57.9	5.76	0.0480
1510	0.141	13.31	53.2	4.73	0.0364
1650	0.129	14.35	49.3	3.91	0.0280

### Mercury Injection Capillary Pressure 07MAW04 - 0.6

#### Table 15 (cont.). MICP data for sample 07MAW04 - 0.6.

	Capillary	Pore Aperture	Э		Incremental	Saturation
	Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
	(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
-						
	1810	0.1179	15.41	45.3	3.99	0.0249
	1980	0.1077	16.42	41.5	3.77	0.0222
	2160	0.0988	17.28	38.3	3.25	0.0181
	2370	0.0900	18.17	34.9	3.32	0.0158
	2590	0.0824	18.93	32.1	2.88	0.0131
	2830	0.0754	19.64	29.4	2.66	0.0111
	3100	0.0688	20.31	26.9	2.51	0.0093
	3390	0.0629	20.92	24.6	2.29	0.0079
	3710	0.0575	21.47	22.5	2.07	0.0065
	4060	0.0525	21.96	20.7	1.85	0.0053
	4440	0.0480	22.41	19.0	1.70	0.0045
	4850	0.0440	22.77	17.7	1.33	0.0032
	5310	0.0402	23.14	16.2	1.40	0.0031
	5810	0.0367	23.47	15.0	1.26	0.0025
	6360	0.0335	23.77	13.9	1.11	0.0020
	6950	0.0307	24.04	12.9	1.03	0.0018
	7610	0.0280	24.28	12.0	0.89	0.0013
	8320	0.0256	24.52	11.1	0.89	0.0012
	9100	0.0234	24.73	10.3	0.81	0.0010
	9960	0.0214	24.95	9.5	0.81	0.0009
	10900	0.0196	25.13	8.8	0.66	0.0007
	11900	0.0179	25.30	8.1	0.66	0.0007
	13000	0.0164	25.48	7.5	0.66	0.0006
	14300	0.0149	25.64	6.9	0.59	0.0005
	15600	0.0137	25.79	6.3	0.59	0.0005
	17100	0.0125	25.95	5.7	0.59	0.0004
	18700	0.0114	26.09	5.2	0.52	0.0003
	20400	0.0105	26.23	4.7	0.52	0.0003
	22300	0.0096	26.34	4.2	0.44	0.0002
	24400	0.0087	26.48	3.7	0.52	0.0002
	26700	0.0080	26.60	3.2	0.44	0.0002
	29300	0.0073	26.72	2.8	0.44	0.0002
	32000	0.0067	26.84	2.4	0.44	0.0002
	35000	0.0061	26.93	2.0	0.37	0.0001
	38300	0.0056	27.03	1.6	0.37	0.0001
	41900	0.0051	27.11	1.3	0.30	0.0001
	45800	0.0047	27.19	1.0	0.30	0.0001
	50100	0.0043	27.27	0.7	0.30	0.0001
	54800	0.0039	27.37	0.4	0.37	0.0001
	59500	0.0036	27.46	0.0	0.37	0.0001

### Mercury Injection Capillary Pressure 07MAW04 - 0.6

Table 16. MICP data for sample 07MAW04 - 10.3.

Sample Informa	<u>tion</u>				
Bulk Volume =	5.7984 cc		Porosity =	23.1% (merury)	
Pore Volume =	1.3388 cc		Permeability =	0.0808 md (mercury)	
Closure = 1.18 9	%BV @ 673 ps	sia	Median Pore Apertu	ure = 0.1095 microns (dia	ameter)
Capillary	Pore Aperture	e		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1.64	130	0.02	100.0	0.00	0.0000
1.80	119	0.02	100.0	0.00	0.0000
1.96	109	0.04	100.0	0.00	0.0000
2.15	99.2	0.06	100.0	0.00	0.0000
2.35	90.8	0.08	100.0	0.00	0.0000
2.57	83.0	0.10	100.0	0.00	0.0000
2.81	75.9	0.10	100.0	0.00	0.0000
3.08	69.3	0.12	100.0	0.00	0.0000
3.37	63.3	0.12	100.0	0.00	0.0000
3.68	58.0	0.14	100.0	0.00	0.0000
4.03	52.9	0.16	100.0	0.00	0.0000
4.41	48.4	0.16	100.0	0.00	0.0000
4.82	44.3	0.18	100.0	0.00	0.0000
5.27	40.5	0.18	100.0	0.00	0.0000
5.77	37.0	0.20	100.0	0.00	0.0000
6.31	33.8	0.20	100.0	0.00	0.0000
6.90	30.9	0.22	100.0	0.00	0.0000
7.55	28.3	0.24	100.0	0.00	0.0000
8.26	25.8	0.24	100.0	0.00	0.0000
9.04	23.6	0.24	100.0	0.00	0.0000
9.89	21.6	0.26	100.0	0.00	0.0000
10.8	19.8	0.28	100.0	0.00	0.0000
11.8	18.1	0.28	100.0	0.00	0.0000
12.9	16.5	0.31	100.0	0.00	0.0000
14.2	15.0	0.31	100.0	0.00	0.0000
15.5	13.8	0.33	100.0	0.00	0.0000
16.9	12.6	0.35	100.0	0.00	0.0000
18.5	11.5	0.35	100.0	0.00	0,0000
20.3	10.5	0.37	100.0	0.00	0,0000
20.0	9.61	0.37	100.0	0.00	0,0000
24.2	8 78	0.30	100.0	0.00	0.0000
24.5	8.02	0.03	100.0	0.00	0.0000
20.0	7 26	0.41	100.0	0.00	0.0000
23.0	6 71	0.43	100.0	0.00	0.0000
2/ 0	6.12	0.45	100.0	0.00	0.0000
34.0 20 0	0.13	0.47	100.0	0.00	0.0000
30.0	0.C	0.49	100.0	0.00	0.0000

# Mercury Injection Capillary Pressure 07MAW04 - 10.3

### Table 16 (cont.). MICP data for sample 07MAW04 - 10.3.

Pressure (psia)         Diameter (microns)         Cumulative Bulk Vol. (%)         Wetting Phase Saturation (%)         Wetting Phase Change (%)         Change (%)         per psia           41.6         5.13         0.49         100.0         0.00         0.000           45.5         4.69         0.53         100.0         0.00         0.000           49.8         4.28         0.53         100.0         0.00         0.000           56.6         3.58         0.53         100.0         0.00         0.000           56.6         3.58         0.55         100.0         0.00         0.0000           71.3         2.99         0.55         100.0         0.00         0.0000           78.0         2.73         0.55         100.0         0.00         0.0000           93.4         2.28         0.57         100.0         0.00         0.0000           122         1.75         0.61         100.0         0.00         0.0000           134         1.59         0.63         100.0         0.00         0.0000           146         1.46         0.63         100.0         0.00         0.0000           157         1.22         0.65 <td< th=""><th>Capillary</th><th>Pore Aperture</th><th>Э</th><th></th><th>Incremental</th><th>Saturation</th></td<>	Capillary	Pore Aperture	Э		Incremental	Saturation
(psia)         (microns)         Bulk Vol. (%)         Saturation (%)         Change (%)         per psia           41.6         5.13         0.49         100.0         0.00         0.0000           45.5         4.69         0.53         100.0         0.00         0.0000           49.8         4.28         0.53         100.0         0.00         0.0000           54.5         3.91         0.53         100.0         0.00         0.0000           55.6         3.58         0.53         100.0         0.00         0.0000           71.3         2.99         0.55         100.0         0.00         0.0000           78.0         2.73         0.55         100.0         0.00         0.0000           93.4         2.28         0.57         100.0         0.00         0.0000           102         2.09         0.59         100.0         0.00         0.0000           122         1.75         0.61         100.0         0.00         0.0000           134         1.59         0.63         100.0         0.00         0.0000           146         1.46         0.65         100.0         0.00         0.0000	Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
41.6       5.13 $0.49$ 100.0 $0.00$ $0.000$ 45.5       4.69 $0.53$ 100.0 $0.00$ $0.000$ 48.8       4.28 $0.53$ 100.0 $0.00$ $0.000$ 54.5       3.91 $0.53$ 100.0 $0.00$ $0.000$ 55.6       3.58 $0.53$ 100.0 $0.00$ $0.000$ 65.2 $3.27$ $0.55$ 100.0 $0.00$ $0.000$ 71.3 $2.99$ $0.55$ 100.0 $0.00$ $0.000$ 78.0 $2.73$ $0.55$ 100.0 $0.00$ $0.000$ 93.4 $2.28$ $0.57$ 100.0 $0.00$ $0.000$ 112       1.90 $0.59$ 100.0 $0.00$ $0.000$ 122       1.75 $0.61$ 100.0 $0.00$ $0.000$ 134       1.59 $0.63$ 100.0 $0.00$ $0.000$ 146       1.46 $0.63$ 100.0 $0.00$ $0.000$ 175       1.22 $0.65$ 100.0 $0.00$	(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
41.6 $5.13$ $0.49$ $100.0$ $0.00$ $0.0000$ 45.5       4.69 $0.53$ $100.0$ $0.00$ $0.0000$ 54.5 $3.91$ $0.53$ $100.0$ $0.00$ $0.0000$ 56.6 $3.58$ $0.53$ $100.0$ $0.00$ $0.0000$ 66.2 $3.27$ $0.55$ $100.0$ $0.00$ $0.0000$ 71.3 $2.99$ $0.55$ $100.0$ $0.00$ $0.0000$ 78.0 $2.73$ $0.55$ $100.0$ $0.00$ $0.0000$ 93.4 $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ 112 $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ 122 $1.75$ $0.61$ $100.0$ $0.00$ $0.0000$ 134 $1.59$ $0.63$ $100.0$ $0.00$ $0.0000$ 146 $1.46$ $0.65$ $100.0$ $0.00$ $0.0000$ 229 $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ 229 $0.932$ $0$						
45.5 $4.69$ $0.53$ $100.0$ $0.00$ $0.0000$ $49.8$ $4.28$ $0.53$ $100.0$ $0.00$ $0.0000$ $54.5$ $3.91$ $0.53$ $100.0$ $0.00$ $0.0000$ $55.6$ $3.58$ $0.53$ $100.0$ $0.00$ $0.0000$ $71.3$ $2.99$ $0.55$ $100.0$ $0.00$ $0.0000$ $78.0$ $2.73$ $0.55$ $100.0$ $0.00$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $102$ $2.09$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ $122$ $1.75$ $0.61$ $100.0$ $0.00$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $290$ $9.32$ $0.69$ $100.0$ $0.00$ $0.0000$ $229$ <	41.6	5.13	0.49	100.0	0.00	0.0000
49.8 $4.28$ $0.53$ $100.0$ $0.00$ $0.0000$ $54.5$ $3.91$ $0.53$ $100.0$ $0.00$ $0.0000$ $59.6$ $3.58$ $0.53$ $100.0$ $0.00$ $0.0000$ $71.3$ $2.99$ $0.55$ $100.0$ $0.00$ $0.0000$ $78.0$ $2.73$ $0.55$ $100.0$ $0.00$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $102$ $2.09$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ $122$ $1.75$ $0.61$ $100.0$ $0.00$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.0000$ $146$ $1.46$ $0.65$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$	45.5	4.69	0.53	100.0	0.00	0.0000
54.5 $3.91$ $0.53$ $100.0$ $0.00$ $0.0000$ $59.6$ $3.58$ $0.53$ $100.0$ $0.000$ $0.0000$ $71.3$ $2.99$ $0.55$ $100.0$ $0.000$ $0.0000$ $78.0$ $2.73$ $0.55$ $100.0$ $0.000$ $0.0000$ $83.3$ $2.50$ $0.57$ $100.0$ $0.000$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $112$ $2.99$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ $122$ $1.75$ $0.61$ $100.0$ $0.00$ $0.0000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ <	49.8	4.28	0.53	100.0	0.00	0.0000
59.6 $3.58$ $0.53$ $100.0$ $0.00$ $0.000$ $65.2$ $3.27$ $0.55$ $100.0$ $0.00$ $0.0000$ $71.3$ $2.99$ $0.55$ $100.0$ $0.00$ $0.0000$ $78.0$ $2.73$ $0.55$ $100.0$ $0.00$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $102$ $2.09$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ $122$ $1.75$ $0.61$ $100.0$ $0.00$ $0.0000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.0000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $254$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $393$ $0.544$ $0.77$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $564$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ <	54.5	3.91	0.53	100.0	0.00	0.0000
65.2 $3.27$ $0.55$ $100.0$ $0.00$ $0.000$ $71.3$ $2.99$ $0.55$ $100.0$ $0.00$ $0.0000$ $85.3$ $2.50$ $0.57$ $100.0$ $0.00$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $102$ $2.09$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.000$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.000$ $0.0000$ $122$ $1.75$ $0.61$ $100.0$ $0.000$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.000$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.000$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.000$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $0.000$ $0.0000$ $615$ <	59.6	3.58	0.53	100.0	0.00	0.0000
71.3 $2.99$ $0.55$ $100.0$ $0.00$ $0.0000$ $78.0$ $2.73$ $0.55$ $100.0$ $0.00$ $0.0000$ $85.3$ $2.50$ $0.57$ $100.0$ $0.00$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $102$ $2.09$ $0.59$ $100.0$ $0.000$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.000$ $0.0000$ $122$ $1.75$ $0.61$ $100.0$ $0.000$ $0.0000$ $134$ $1.59$ $0.63$ $100.0$ $0.000$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.000$ $0.0000$ $160$ $1.33$ $0.63$ $100.0$ $0.000$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.000$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.000$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.000$ $0.0000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.73$ $100.0$ $0.000$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.000$ $0.0000$ $333$ $0.543$ $0.81$ $100.0$ $0.000$ $0.0000$ $347$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$	65.2	3.27	0.55	100.0	0.00	0.0000
78.0 $2.73$ $0.55$ $100.0$ $0.00$ $0.0000$ $85.3$ $2.50$ $0.57$ $100.0$ $0.00$ $0.0000$ $93.4$ $2.28$ $0.57$ $100.0$ $0.00$ $0.0000$ $102$ $2.09$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.0000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.0000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.0000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $330$ $0.543$ $0.85$ $100.0$ $0.00$ $0.0000$ $393$ $0.543$ $0.85$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $514$ $0.377$ $1.06$ $100.0$ $0.00$ $0.0000$ $514$ $0.347$ $1.06$ $100.0$ $0.00$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.00$ $0.0000$ <	71.3	2.99	0.55	100.0	0.00	0.0000
85.3         2.50         0.57         100.0         0.00         0.0000           93.4         2.28         0.57         100.0         0.00         0.0000           102         2.09         0.59         100.0         0.00         0.0000           112         1.90         0.59         100.0         0.00         0.0000           122         1.75         0.61         100.0         0.00         0.0000           134         1.59         0.63         100.0         0.00         0.0000           146         1.46         0.63         100.0         0.00         0.0000           160         1.33         0.63         100.0         0.00         0.0000           175         1.22         0.65         100.0         0.00         0.0000           209         1.02         0.67         100.0         0.00         0.0000           229         0.932         0.69         100.0         0.00         0.0000           251         0.850         0.71         100.0         0.00         0.0000           300         0.711         100.0         0.00         0.0000           328         0.650         0.75 <td>78.0</td> <td>2.73</td> <td>0.55</td> <td>100.0</td> <td>0.00</td> <td>0.0000</td>	78.0	2.73	0.55	100.0	0.00	0.0000
93.4 $2.28$ $0.57$ $100.0$ $0.00$ $0.000$ $102$ $2.09$ $0.59$ $100.0$ $0.00$ $0.000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.000$ $112$ $1.75$ $0.61$ $100.0$ $0.00$ $0.000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.0000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $254$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.75$ $100.0$ $0.00$ $0.0000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $514$ $0.415$ $0.99$ $100.0$ $0.000$ $0.0000$ $514$ $0.415$ $0.94$ $100.0$ $0.000$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.000$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.000$ $0.0000$ <	85.3	2.50	0.57	100.0	0.00	0.0000
102 $2.09$ $0.59$ $100.0$ $0.00$ $0.000$ $112$ $1.90$ $0.59$ $100.0$ $0.00$ $0.000$ $122$ $1.75$ $0.61$ $100.0$ $0.00$ $0.000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.75$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.0000$ $393$ $0.543$ $0.81$ $100.0$ $0.00$ $0.0000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.0000$ $470$ $0.454$ $0.94$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.00$ $0.0000$ $615$ $0.242$ $1.83$ $97.2$ $1.32$ $0.176$ $964$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ $150$ $0.166$ $1.592$ $79.5$ $7.58$ $0.6689$ $1380$ <	93.4	2.28	0.57	100.0	0.00	0.0000
112 $1.90$ $0.59$ $100.0$ $0.00$ $0.000$ $122$ $1.75$ $0.61$ $100.0$ $0.00$ $0.000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.000$ $146$ $1.33$ $0.63$ $100.0$ $0.00$ $0.000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.0000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.000$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.000$ $0.0000$ <t< td=""><td>102</td><td>2.09</td><td>0.59</td><td>100.0</td><td>0.00</td><td>0.0000</td></t<>	102	2.09	0.59	100.0	0.00	0.0000
122 $1.75$ $0.61$ $100.0$ $0.00$ $0.000$ $134$ $1.59$ $0.63$ $100.0$ $0.00$ $0.000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.0000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.0000$ $393$ $0.543$ $0.81$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.32$ $99.4$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $811$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ $9$	112	1.90	0.59	100.0	0.00	0.0000
134 $1.59$ $0.63$ $100.0$ $0.00$ $0.000$ $146$ $1.46$ $0.63$ $100.0$ $0.00$ $0.000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.0000$ $191$ $1.12$ $0.65$ $100.0$ $0.00$ $0.0000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.0000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.0000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.0000$ $300$ $0.711$ $0.75$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.0000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.06$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.32$ $99.4$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.126$ $8$	122	1.75	0.61	100.0	0.00	0.0000
146 $1.46$ $0.63$ $100.0$ $0.00$ $0.000$ $160$ $1.33$ $0.63$ $100.0$ $0.00$ $0.000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.000$ $0.0000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.0000$ $393$ $0.543$ $0.81$ $100.0$ $0.000$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $470$ $0.454$ $0.90$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $615$ $0.347$ $1.66$ $100.0$ $0.000$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.000$ $0.0000$ $736$ $0.290$ $1.32$ $99.4$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $811$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ <td< td=""><td>134</td><td>1.59</td><td>0.63</td><td>100.0</td><td>0.00</td><td>0.0000</td></td<>	134	1.59	0.63	100.0	0.00	0.0000
160 $1.33$ $0.63$ $100.0$ $0.00$ $0.000$ $175$ $1.22$ $0.65$ $100.0$ $0.00$ $0.000$ $191$ $1.12$ $0.65$ $100.0$ $0.00$ $0.000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.0000$ $274$ $0.779$ $0.71$ $100.0$ $0.000$ $0.0000$ $300$ $0.711$ $0.73$ $100.0$ $0.000$ $0.0000$ $328$ $0.650$ $0.75$ $100.0$ $0.000$ $0.0000$ $359$ $0.594$ $0.77$ $100.0$ $0.000$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.000$ $0.0000$ $470$ $0.454$ $0.90$ $100.0$ $0.000$ $0.0000$ $514$ $0.415$ $0.94$ $100.0$ $0.000$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.000$ $0.0000$ $615$ $0.347$ $1.66$ $100.0$ $0.000$ $0.0000$ $673$ $0.217$ $1.32$ $9.44$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $881$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ $964$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ <	146	1.46	0.63	100.0	0.00	0.0000
175 $1.22$ $0.65$ $100.0$ $0.00$ $0.000$ $191$ $1.12$ $0.65$ $100.0$ $0.00$ $0.000$ $209$ $1.02$ $0.67$ $100.0$ $0.00$ $0.000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.0000$ $615$ $0.347$ $1.66$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.0000$ $736$ $0.290$ $1.32$ $99.4$ $0.62$ $0.0998$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $881$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ $1050$ $0.203$ $2.99$ $92.2$ $2.73$ $0.0318$ $115$	160	1.33	0.63	100.0	0.00	0.0000
191 $1.12$ $0.65$ $100.0$ $0.00$ $0.000$ 209 $1.02$ $0.67$ $100.0$ $0.00$ $0.000$ 229 $0.932$ $0.69$ $100.0$ $0.00$ $0.000$ 251 $0.850$ $0.71$ $100.0$ $0.00$ $0.000$ 274 $0.779$ $0.71$ $100.0$ $0.00$ $0.000$ 300 $0.711$ $0.73$ $100.0$ $0.00$ $0.000$ 328 $0.650$ $0.75$ $100.0$ $0.00$ $0.000$ 359 $0.594$ $0.77$ $100.0$ $0.00$ $0.000$ 393 $0.543$ $0.81$ $100.0$ $0.00$ $0.000$ 430 $0.496$ $0.85$ $100.0$ $0.00$ $0.000$ 430 $0.496$ $0.85$ $100.0$ $0.00$ $0.000$ 514 $0.415$ $0.94$ $100.0$ $0.00$ $0.000$ 563 $0.379$ $1.00$ $100.0$ $0.00$ $0.000$ 673 $0.317$ $1.18$ $100.0$ $0.00$ $0.000$ 673 $0.290$ $1.32$ $99.4$ $0.62$ $0.0098$ 806 $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ 881 $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ 964 $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ $1050$ $0.203$ $2.99$ $92.2$ $2.73$ $0.318$ $1150$ $0.186$ $4.17$ $87.0$ $5.11$ $0.0617$ $1380$ $0.155$ $7.71$	175	1.22	0.65	100.0	0.00	0.0000
209 $1.02$ $0.67$ $100.0$ $0.00$ $0.000$ $229$ $0.932$ $0.69$ $100.0$ $0.00$ $0.000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.000$ $393$ $0.543$ $0.81$ $100.0$ $0.00$ $0.000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.000$ $673$ $0.317$ $1.18$ $100.0$ $0.000$ $0.0000$ $736$ $0.290$ $1.32$ $99.4$ $0.62$ $0.0098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $881$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ $1050$ $0.203$ $2.99$ $92.2$ $2.73$ $0.0318$ $1150$ $0.186$ $4.17$ $87.0$ $5.11$ $0.0617$ $1380$ $0.155$ $7.71$ $71.7$ $7.58$ $0.0689$ $1380$	191	1.12	0.65	100.0	0.00	0.0000
229 $0.932$ $0.69$ $100.0$ $0.00$ $0.000$ $251$ $0.850$ $0.71$ $100.0$ $0.00$ $0.000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.000$ $393$ $0.543$ $0.81$ $100.0$ $0.00$ $0.0000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.0000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.0000$ $514$ $0.415$ $0.94$ $100.0$ $0.00$ $0.0000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.0000$ $615$ $0.347$ $1.06$ $100.0$ $0.00$ $0.0000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.0000$ $736$ $0.290$ $1.32$ $99.4$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $811$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ $964$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ $1050$ $0.203$ $2.99$ $92.2$ $2.73$ $0.0318$ $1150$ $0.186$ $4.17$ $87.0$ $5.11$ $0.05116$ $1260$ $0.169$ $5.92$ $79.5$ $7.58$ $0.0689$ <td< td=""><td>209</td><td>1.02</td><td>0.67</td><td>100.0</td><td>0.00</td><td>0.0000</td></td<>	209	1.02	0.67	100.0	0.00	0.0000
251 $0.850$ $0.71$ $100.0$ $0.00$ $0.000$ $274$ $0.779$ $0.71$ $100.0$ $0.00$ $0.000$ $300$ $0.711$ $0.73$ $100.0$ $0.00$ $0.000$ $328$ $0.650$ $0.75$ $100.0$ $0.00$ $0.000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.000$ $393$ $0.543$ $0.81$ $100.0$ $0.00$ $0.000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.000$ $514$ $0.415$ $0.94$ $100.0$ $0.00$ $0.000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.000$ $615$ $0.347$ $1.06$ $100.0$ $0.00$ $0.000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.000$ $736$ $0.290$ $1.32$ $99.4$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $881$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ $964$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ $1050$ $0.203$ $2.99$ $92.2$ $2.73$ $0.0318$ $1150$ $0.186$ $4.17$ $87.0$ $5.11$ $0.0511$ $1260$ $0.169$ $5.92$ $79.5$ $7.58$ $0.0689$ $1380$ $0.155$ $7.71$ $71.7$ $7.76$ $0.0647$ $1510$	229	0.932	0.69	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	251	0.850	0.71	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	274	0.779	0.71	100.0	0.00	0.0000
328 $0.650$ $0.75$ $100.0$ $0.00$ $0.000$ $359$ $0.594$ $0.77$ $100.0$ $0.00$ $0.000$ $393$ $0.543$ $0.81$ $100.0$ $0.00$ $0.000$ $430$ $0.496$ $0.85$ $100.0$ $0.00$ $0.000$ $470$ $0.454$ $0.90$ $100.0$ $0.00$ $0.000$ $514$ $0.415$ $0.94$ $100.0$ $0.00$ $0.000$ $563$ $0.379$ $1.00$ $100.0$ $0.00$ $0.000$ $615$ $0.347$ $1.06$ $100.0$ $0.00$ $0.000$ $673$ $0.317$ $1.18$ $100.0$ $0.00$ $0.000$ $736$ $0.290$ $1.32$ $99.4$ $0.62$ $0.098$ $806$ $0.265$ $1.53$ $98.5$ $0.88$ $0.0126$ $881$ $0.242$ $1.83$ $97.2$ $1.32$ $0.0176$ $964$ $0.221$ $2.36$ $94.9$ $2.29$ $0.0276$ $1050$ $0.203$ $2.99$ $92.2$ $2.73$ $0.0318$ $1150$ $0.186$ $4.17$ $87.0$ $5.11$ $0.0511$ $1260$ $0.169$ $5.92$ $79.5$ $7.58$ $0.0689$ $1380$ $0.155$ $7.71$ $71.7$ $7.76$ $0.0647$ $1510$ $0.141$ $9.26$ $65.0$ $6.70$ $0.0516$ $1650$ $0.129$ $10.64$ $59.0$ $6.00$ $0.0428$	300	0.711	0.73	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	328	0.650	0.75	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	359	0.594	0.77	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	393	0.543	0.81	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	430	0.496	0.85	100.0	0.00	0.0000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	470	0.454	0.90	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	514	0.415	0.94	100.0	0.00	0.0000
	563	0.379	1.00	100.0	0.00	0.0000
	615	0.347	1.06	100.0	0.00	0.0000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	673	0.317	1.18	100.0	0.00	0.0000
806         0.265         1.53         98.5         0.88         0.0126           881         0.242         1.83         97.2         1.32         0.0176           964         0.221         2.36         94.9         2.29         0.0276           1050         0.203         2.99         92.2         2.73         0.0318           1150         0.186         4.17         87.0         5.11         0.0511           1260         0.169         5.92         79.5         7.58         0.0689           1380         0.155         7.71         71.7         7.76         0.0647           1510         0.141         9.26         65.0         6.70         0.0516           1650         0.129         10.64         59.0         6.00         0.0428	736	0.290	1.32	99.4	0.62	0.0098
881         0.242         1.83         97.2         1.32         0.0176           964         0.221         2.36         94.9         2.29         0.0276           1050         0.203         2.99         92.2         2.73         0.0318           1150         0.186         4.17         87.0         5.11         0.0511           1260         0.169         5.92         79.5         7.58         0.0689           1380         0.155         7.71         71.7         7.76         0.0647           1510         0.141         9.26         65.0         6.70         0.0516           1650         0.129         10.64         59.0         6.00         0.0428	806	0.265	1.53	98.5	0.88	0.0126
964         0.221         2.36         94.9         2.29         0.0276           1050         0.203         2.99         92.2         2.73         0.0318           1150         0.186         4.17         87.0         5.11         0.0511           1260         0.169         5.92         79.5         7.58         0.0689           1380         0.155         7.71         71.7         7.76         0.0647           1510         0.141         9.26         65.0         6.70         0.0516           1650         0.129         10.64         59.0         6.00         0.0428	881	0.242	1.83	97.2	1.32	0.0176
10500.2032.9992.22.730.031811500.1864.1787.05.110.051112600.1695.9279.57.580.068913800.1557.7171.77.760.064715100.1419.2665.06.700.051616500.12910.6459.06.000.0428	964	0.221	2.36	94.9	2.29	0.0276
11500.1864.1787.05.110.051112600.1695.9279.57.580.068913800.1557.7171.77.760.064715100.1419.2665.06.700.051616500.12910.6459.06.000.0428	1050	0.203	2.99	92.2	2.73	0.0318
12600.1695.9279.57.580.068913800.1557.7171.77.760.064715100.1419.2665.06.700.051616500.12910.6459.06.000.0428	1150	0.186	4.17	87.0	5.11	0.0511
1380         0.155         7.71         71.7         7.76         0.0647           1510         0.141         9.26         65.0         6.70         0.0516           1650         0.129         10.64         59.0         6.00         0.0428	1260	0.169	5.92	79.5	7.58	0.0689
1510         0.141         9.26         65.0         6.70         0.0516           1650         0.129         10.64         59.0         6.00         0.0428	1380	0.155	7.71	71.7	7.76	0.0647
1650 0.129 10.64 59.0 6.00 0.0428	1510	0.141	9.26	65.0	6.70	0.0516
	1650	0.129	10.64	59.0	6.00	0.0428

## Mercury Injection Capillary Pressure 07MAW04 - 10.3

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#### Table 16 (cont.). MICP data for sample 07MAW04 - 10.3.

Capillary	Pore Apertur	e		Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
1810	0.1179	11.84	53.8	5.20	0.0325
1980	0.1077	12.90	49.2	4.59	0.0270
2160	0.0988	13.81	45.2	3.97	0.0220
2370	0.0900	14.69	41.4	3.79	0.0181
2590	0.0824	15.42	38.3	3.17	0.0144
2830	0.0754	16.09	35.4	2.91	0.0121
3100	0.0688	16.70	32.7	2.65	0.0098
3390	0.0629	17.23	30.4	2.29	0.0079
3710	0.0575	17.72	28.3	2.12	0.0066
4060	0.0525	18.17	26.4	1.94	0.0055
4440	0.0480	18.57	24.6	1.76	0.0046
4850	0.0440	18.92	23.1	1.50	0.0037
5310	0.0402	19.27	21.6	1.50	0.0033
5810	0.0367	19.59	20.2	1.41	0.0028
6360	0.0335	19.90	18.9	1.32	0.0024
6950	0.0307	20.18	17.6	1.23	0.0021
7610	0.0280	20.45	16.5	1.15	0.0017
8320	0.0256	20.71	15.3	1.15	0.0016
9100	0.0234	20.95	14.3	1.06	0.0014
9960	0.0214	21.18	13.3	0.97	0.0011
10900	0.0196	21.40	12.3	0.97	0.0010
11900	0.0179	21.60	11.5	0.88	0.0009
13000	0.0164	21.81	10.6	0.88	0.0008
14300	0.0149	22.01	9.7	0.88	0.0007
15600	0.0137	22.17	9.0	0.71	0.0005
17100	0.0125	22.36	8.2	0.79	0.0005
18700	0.0114	22.52	7.5	0.71	0.0004
20400	0.0105	22.68	6.8	0.71	0.0004
22300	0.0096	22.85	6.1	0.71	0.0004
24400	0.0087	22.99	5.5	0.62	0.0003
26700	0.0080	23.13	4.9	0.62	0.0003
29300	0.0073	23.29	4.1	0.71	0.0003
32000	0.0067	23.42	3.6	0.53	0.0002
35000	0.0061	23.54	3.1	0.53	0.0002
38300	0.0056	23.66	2.6	0.53	0.0002
41900	0.0051	23.78	2.0	0.53	0.0001
45800	0.0047	23.88	1.6	0.44	0.0001
50100	0.0043	23.99	1.1	0.44	0.0001
54800	0.0039	24.13	0.5	0.62	0.0001
59500	0.0036	24.25	0.0	0.53	0.0001

# Mercury Injection Capillary Pressure 07MAW04 - 10.3

Table 17. MICP data for sample ST4 - 20.

Sample Information								
Bulk Volume =	5.3015 cc		Porosity =	35.7% (mercury)				
Pore Volume =	1.8914 cc		Permeability =	0.215 md (mercury	)			
Closure = 1.01 %BV @ 470 psia Median Pore Aperture = 0.1308 microns (diameter)								
Capillary	Pore Aperture			Incremental	Saturation			
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change			
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia			
4.04	100		100.0	0.00	0.0000			
1.64	130	0.02	100.0	0.00	0.0000			
1.80	119	0.02	100.0	0.00	0.0000			
1.96	109	0.03	100.0	0.00	0.0000			
2.15	99.2	0.03	100.0	0.00	0.0000			
2.35	90.8	0.05	100.0	0.00	0.0000			
2.57	83.0	0.05	100.0	0.00	0.0000			
2.81	75.9	0.05	100.0	0.00	0.0000			
3.08	69.3	0.07	100.0	0.00	0.0000			
3.37	63.3	0.07	100.0	0.00	0.0000			
3.68	58.0	0.07	100.0	0.00	0.0000			
4.03	52.9	0.09	100.0	0.00	0.0000			
4.41	48.4	0.09	100.0	0.00	0.0000			
4.82	44.3	0.09	100.0	0.00	0.0000			
5.27	40.5	0.09	100.0	0.00	0.0000			
5.77	37.0	0.09	100.0	0.00	0.0000			
6.31	33.8	0.09	100.0	0.00	0.0000			
6.90	30.9	0.09	100.0	0.00	0.0000			
7.55	28.3	0.09	100.0	0.00	0.0000			
8.26	25.8	0.09	100.0	0.00	0.0000			
9.04	23.6	0.09	100.0	0.00	0.0000			
9.89	21.6	0.09	100.0	0.00	0.0000			
10.8	19.8	0.09	100.0	0.00	0.0000			
11.8	18.1	0.09	100.0	0.00	0.0000			
12.9	16.5	0.09	100.0	0.00	0.0000			
14.2	15.0	0.09	100.0	0.00	0.0000			
15.5	13.8	0.09	100.0	0.00	0.0000			
16.9	12.6	0.09	100.0	0.00	0.0000			
18.5	11.5	0.09	100.0	0.00	0.0000			
20.3	10.5	0.09	100.0	0.00	0.0000			
22.2	9.61	0.20	100.0	0.00	0.0000			
24.3	8.78	0.20	100.0	0.00	0.0000			
26.6	8.02	0.22	100.0	0.00	0.0000			
29.0	7.36	0.22	100.0	0.00	0.0000			
31.8	6.71	0.24	100.0	0.00	0.0000			
34.8	6.13	0.26	100.0	0.00	0.0000			
38.0	5.61	0.26	100.0	0.00	0.0000			

# Mercury Injection Capillary Pressure ST4 - 20

Table 17 (cont.). MICP data for sample ST4 - 20.

Capillary	Pore Aperture			Incremental	Saturation
Pressure	Diameter	Cumulative	Wetting Phase	Wetting Phase	Change
(psia)	(microns)	Bulk Vol. (%)	Saturation (%)	Change (%)	per psia
41.6	5.13	0.27	100.0	0.00	0.0000
45.5	4.69	0.29	100.0	0.00	0.0000
49.8	4.28	0.29	100.0	0.00	0.0000
54.5	3.91	0.29	100.0	0.00	0.0000
59.6	3.58	0.29	100.0	0.00	0.0000
65.2	3.27	0.29	100.0	0.00	0.0000
71.3	2.99	0.29	100.0	0.00	0.0000
78.0	2.73	0.31	100.0	0.00	0.0000
85.3	2.50	0.31	100.0	0.00	0.0000
93.4	2.28	0.31	100.0	0.00	0.0000
102	2.09	0.31	100.0	0.00	0.0000
112	1.90	0.31	100.0	0.00	0.0000
122	1.75	0.32	100.0	0.00	0.0000
134	1.59	0.32	100.0	0.00	0.0000
146	1.46	0.34	100.0	0.00	0.0000
160	1.33	0.36	100.0	0.00	0.0000
175	1.22	0.38	100.0	0.00	0.0000
191	1.12	0.43	100.0	0.00	0.0000
209	1.02	0.44	100.0	0.00	0.0000
229	0.932	0.48	100.0	0.00	0.0000
251	0.850	0.49	100.0	0.00	0.0000
274	0.779	0.53	100.0	0.00	0.0000
300	0.711	0.58	100.0	0.00	0.0000
328	0.650	0.63	100.0	0.00	0.0000
359	0.594	0.68	100.0	0.00	0.0000
393	0.543	0.77	100.0	0.00	0.0000
430	0.496	0.87	100.0	0.00	0.0000
470	0.454	1.01	100.0	0.00	0.0000
514	0.415	1.19	99.5	0.53	0.0120
563	0.379	1.50	98.6	0.86	0.0176
615	0.347	1.88	97.6	1.05	0.0202
673	0.317	2.28	96.4	1.15	0.0198
736	0.290	2.90	94.7	1.72	0.0273
806	0.265	3.31	93.5	1.15	0.0164
881	0.242	3.99	91.6	1.91	0.0255
964	0.221	4.84	89.2	2.39	0.0288
1050	0.203	5.88	86.3	2.92	0.0339
1150	0.186	7.47	81.9	4.45	0.0445
1260	0.169	10.11	74.5	7.41	0.0674
1380	0.155	13.19	65.8	8.66	0.0721
1510	0.141	17.03	55.0	10.76	0.0828
1650	0.129	19.16	49.1	5.98	0.0427

## Mercury Injection Capillary Pressure ST4 - 20

### Table 17 (cont.). MICP data for sample ST4 - 20.

Capillary	Pore Aperture	Cumulativa	Watting Dhoop	Incremental	Saturation
(psia)	(microns)		Saturation (%)	Change (%)	change
(psia)	(11101013)	Duik VOI. (70)	Saturation (70)	Change (70)	
1810	0 1170	21 10	13.6	5 15	0.03/1
1980	0.1077	21.10	39.0	1 59	0.0341
2160	0.1077	24.07	35.3	3 73	0.0270
2370	0.0900	25.28	31.9	3 40	0.0207
2590	0.0824	26.32	29.0	2 92	0.0133
2830	0.0021	27.24	26.4	2.58	0.0108
3100	0.0688	28.11	24.0	2 44	0.0090
3390	0.0629	28.84	21.9	2.06	0.0071
3710	0.0575	29.52	20.0	1.91	0.0060
4060	0.0525	30.12	18.3	1.67	0.0048
4440	0.0480	30.65	16.8	1.48	0.0039
4850	0.0440	31.08	15.6	1.20	0.0029
5310	0.0402	31.50	14.4	1.20	0.0026
5810	0.0367	31.88	13.4	1.05	0.0021
6360	0.0335	32.20	12.5	0.91	0.0017
6950	0.0307	32.51	11.6	0.86	0.0015
7610	0.0280	32.78	10.9	0.77	0.0012
8320	0.0256	33.02	10.2	0.67	0.0009
9100	0.0234	33.24	9.6	0.62	0.0008
9960	0.0214	33.44	9.0	0.57	0.0007
10900	0.0196	33.65	8.4	0.57	0.0006
11900	0.0179	33.84	7.9	0.53	0.0005
13000	0.0164	34.02	7.4	0.53	0.0005
14300	0.0149	34.21	6.8	0.53	0.0004
15600	0.0137	34.38	6.4	0.48	0.0004
17100	0.0125	34.55	5.9	0.48	0.0003
18700	0.0114	34.72	5.4	0.48	0.0003
20400	0.0105	34.88	5.0	0.43	0.0003
22300	0.0096	35.03	4.5	0.43	0.0002
24400	0.0087	35.20	4.1	0.48	0.0002
26700	0.0080	35.35	3.6	0.43	0.0002
29300	0.0073	35.51	3.2	0.43	0.0002
32000	0.0067	35.64	2.8	0.38	0.0001
35000	0.0061	35.80	2.4	0.43	0.0001
38300	0.0056	35.93	2.0	0.38	0.0001
41900	0.0051	36.05	1.7	0.33	0.0001
45800	0.0047	36.19	1.3	0.38	0.0001
50100	0.0043	36.34	0.9	0.43	0.0001
54800	0.0039	36.51	0.4	0.48	0.0001
59500	0.0036	36.65	0.0	0.38	0.0001

### Mercury Injection Capillary Pressure ST4 - 20